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UH-1 AND AH-1 HELICOPTER MAIN ROTOR BLADE FAILURE AND SCRAP RATE DATA ANALYSIS

P. Y. Carr O. L. Hensley

January 1971

EUSTIS DIRECTORATE U. S. ARMY AIR MOBILITY RESEARCH AND DEVELOPMENT LABORATORY FORT EUSTIS, VIRGINIA

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BELL HELICOPTER COMPANY
FORT WORTH, TEXAS

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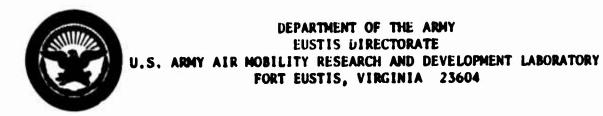
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Preliminary studies of the impact of the Army's operational environment on helicopter rotor blade failure rates indicate that external causes (combat damage, etc.) are considerably greater than causes associated with blade design (fatigue failure, etc.). This contract was initiated to assess the impact of the Army's operational environment on the scrap and failure rate of UH-1 and AH-1 series main rotor blades. Results reported herein show that the Army is experiencing very high maintenance support costs primarily due to extremely poor repairability characteristics. The need for design concepts with a high degree of field repairability is evident. These findings suggest that a highly repairable blade concept incorporating replaceable blade segments or a relatively cheap, expendable rotor blade concept may prove fruitful. Design studies of these concepts are currently under way. This report is published to assist designers of rotor systems by providing a better understanding of the reasons for blade failure and the distribution according to operational conditions.

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By

P.V. Carr O.L. Hensley

Prepared by

Bell Helicopter Company Fort Worth, Texas

for

EUSTIS DIRECTORATE U. S. ARMY AIR MOBILITY RESEARCH AND DEVELOPMENT LABORATORY FORT EUSTIS, VIRGINIA

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ABSTRACT

This report presents the results of an investigation of the impact of the Army's operational environment on UH-1 and AH-1 series main rotor blades. Thirty-nine months of operational data for missions flown in the United States as well as in Southeast Asia under actual combat conditions were reviewed and reported. Blade failures are reported in terms of cause, frequency, repairability, and probability of blade scrappage following removal. The maintenance man-hours associated with each type of repair, the most forward area at which repairs may be accomplished, and the associated downtimes and support costs are reported. Repair, overhaul, and new blade costs are converted to operational costs in dollars per flight hour. The concepts of blades with a high degree of field repairability and "throwaway" blades are discussed. Target new blade costs at which such concepts become cost effective are developed.



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I. SUMMARY

The main rotor blade analysis was conducted and this report was prepared under Contract DAAJ02-70-C-0016. Analysis of premature removal, time change, repair and scrap data was conducted on the two types of the UH-1/AH-1 series aircraft main rotor blades shown in Table I.

l'ABLE I. MAIN ROTOR BLADES ANALYZED

Blade Part No.	Models Used On	Cost of* New Blade	Allowable Operating Time			
204-011-250-5	UH-1D/UH-1H	\$2918.19	2500 hours			
540-011-001-5	UH-1C/AH-1G	\$3151.71	1100 hours			
* Contract DAAJ01-68-A-0022, Spare Parts Cost List						

The results of the analysis to determine the mean-time-toremoval (MTR) and mean-time-between-removals (MTBR) are shown in Table II. Values are expressed in blade hours.

TABLE II. MTR AND MTBF VALUES FOR MAIN ROTOR BLADES

	Combat Area		CONUS Area		
Blade Part No.	Reason For Removal	MTR	MTBR	MTR	MTBR
204-011-250-5	All Part Causes External Causes	1 ₄₀₉ 520 369	⁵ 1063 5560 1326	³ 993 994 766	7 720 1919 2879
540-011-001-5	All Part Causes External Causes	² 316 371 272	6 908 3602 1252	4476 455 290	⁸ 1449 2974 4036

- Based on 4609 blade removals, TAERS Data.
- Based on 1288 blade removals, TAERS Data. 2.
- Based on 333 blade removals, TAERS Data. Based on 53 blade removals, TAERS Data.
- Based on 136 removals and 144,556 blade hours, TAERS Data.
- Based on 250 removals and 226,920 blade hours, TAERS Data.
- Based on 16 removals and 11,516 blade hours, TAERS Data.
- Based on 39 removals and 56,508 blade hours, M & R Data.

The MTR/MTBR values are for blades removed during the period from 1966 through 1969. The MTR's for the combat area (Vietnam) are sensitive to combat intensity during shorter periods.

The results of the scrappage data analyses are shown in Tables III and IV.

TABLE III. REASON FOR REMOVAL VERSUS REASON FOR SCRAPPAGE* AT A BLADE REPAIR FACILITY

(As a percentage of the total number of blades that were scrapped)

Blade Part No. 204-011-250-5 (UH-1D/H)						
		Reason For Removal				
Reason For Scrappage	All Causes	Part Causes	External Causes	No Failure Causes	Unknown Caus es	
All Causes	100.00%	20.50%	41.19%	1.76%	36.55%	
Part Causes	73.38%	17.61%	26.83%	1.48%	27.46%	
External Causes	24.16%	2.68%	13.73%	0.28%	7.47%	
Time Change	0.28%	0.00%	0.14%	0.00%	0.14%	
Other	2.18%	0.21%	0.49%	0.00%	1.48%	
Blade	Part No	. 540-0	L1-001-5	(UH-1G/AH-10	G)	
Reason For Scrappage	All Causes	Part Causes	External Causes	No Failure Causes	Unknown Causes	
All Causes	100.00%	15.54%	55.13%	6.16%	23.17%	
Part Causes	29.91%	8.50%	11.44%	1.17%	8.80%	
External Causes	56.89%	4.69%	40.76%	0.59%	10.85%	
Time Change	5.87%	1.76%	0.00%	3.52%	0.59%	
Other	7.33%	0.59%	2.93%	0.88%	2.93%	
* From BHC Blade Repair Facility Data						

TABLE IV. PROBABILITY OF SCRAPPAGE OF MAIN ROTOR BLADES REMOVED IN VIETNAM

		Probability of Scrappage Range (90% Confidence)		
Blade Part No.	Reason For Removal	Of Total Blades Removed	At the Removal Location	Of Blades Shipped For Repair
204-011-250-5 (UH-1D/H)	Both Causes Part Causes External Causes	65.8-74.1 51.1-66.9 70.0-79.4	14.7-27.6	62.1-73.2 54.1-73.7 62.5-75.9
540-011-001-5 (UH-1C/AH-1G)	Both Causes Part Causes External Causes	71.5-79.2 63.0-84.1 71.3-79.6	49.7-58.6 40.1-64.2 49.6-59.2	Name and the second

By the time the blades arrive at a blade repair facility most of the blades that were obviously not reparable were scrapped. The blades that are scrapped at the repair facility are blades with defects that can be seen only when the blades are disassembled or at least given an inspection more detailed than the previous one. The reasons for blade scrappage at a repair facility may therefore differ from the reasons for removal. Prior to the blades reaching a repair facility the reason for scrappage of a blade is usually consistent with its reason for removal. Exceptions to this are the blades that are damaged during or after removal.

The Probability of Scrappage analysis considered 331 UH-1D/H blade removals during the Julian calendar period 7200 through 7299 and 336 UH-1C/AH-1G blade removals during the period 7200 through 8099. The UH-1C/AH-1G blades show a greater probability of scrappage at the point of removal than do the UH-1D/H blades, while the scrappage probabilities of the blades shipped for repair are comparable.

The results of the analysis of main-rotor-blade support-costs is shown in Table V (based on a 5000-hour aircraft life cycle).

TABLE V. MAIN ROTOR BLADE SUPPORT COSTS FOR AIRCRAFT STATIONED IN VIETNAM

	New Rep	ing lacement s Only	Using Both New & Repaired Blades
Blade Part No.	* Minimum Cost \$/Flt. Hr.	** Maximum Cost \$/Flt. Hr.	*** Estimated Cost \$/Flt. Hr.
204-011-250-5 (UH-1D/H)	\$10.73	\$12.14	\$10.02
540-011-001-5 (UH-1C/AH-1G)	15.32	18.00	14.81

- * Based on the replacement of all blades not reparable at point of removal with new blades
- ** Based on the new blade replacement and no blade repair
- *** Based on air transport of damaged blades to CONUS and new and repaired blades to Vietnam

The existing program of blade repair even with the large percentage of scrapped blades is cost effective, about two to four dollars per flight hour less expensive than the support cost would be if no blades were repaired. It is \$0.51 to \$0.71 less expensive than the support cost would be if the blade repairs were limited to those that could be accomplished at the point of removal. If the percentage of repairs at the point of removal could be increased sufficiently, it would become cost effective to eliminate the repair programs at CONUS facilities.

II. INTRODUCTION

This report was prepared in accordance with the requirements of Contract DAAJ02-70-C-0016, UH-1 and AH-1 Helicopter Rotor Blade Failure and Scrap Rate Data Analysis.

The purpose was to conduct an analysis of UH-1 and AH-1 series helicopter main rotor blade failures and scrappage. The analysis treats the data in two major groups.

- The UH-ID/H main rotor blades
- The UH-1C/AH-1G main rotor blades

In the case of the UH-ID/H, the analysis considers only the improved version of the blades currently used. All blades used on the UH-IC/AH-IG are of improved design.

The analysis also develops the following:

- Mean-time-to-removal (MTR) and mean-time-between removals (MTBR) under combat and noncombat conditions
 - . Due to part causes
 - . Due to external causes
- Probability of scrappage for blades removed in combat areas for part and external causes
- A correlation of the reasons for removal in the field and the reason for scrappage at a blade repair facility
- Aircraft support costs in dollars per flight hour for main rotor blades

The analyses in this report provide a basis for evaluation of MTR, MTBR, reparability, and rotor blade support cost characteristics of future blade designs.

III. ANALYSIS APPROACH

A. DATA FILES

Bell Helicopter Company (BHC) has four main sources of main rotor blade failure, removal, repair, and scrap data. They are:

1. The Army Equipment Record System (TAERS) DA2410, Component Removal and Repair/Overhaul Record Data

These data are supplied on magnetic tape to BHC as Government Furnished data under the UH-1/AH-1 Maintainability and Reliability (M & R) Program, Contract DAAJ01-67-C-1588(G). Limited computer programs were developed under the M & R Program to sort, select and list the TAERS data.

2. The Field Failure/Discrepancy Report (FDR) Data

These data were reported by Reliability Field Engineers who monitored groups of UH-1C/D/H and AH-1G helicopters under provisions of the UH-1/AH-1 M & R Program. Computer programs developed under the M & R Program group, list, and sum the data by failure mode.

3. The Disassembly Inspection Summary, OSM-634 Form Data

This is a government form on which BHC reports the overhaul, repair and scrappage of overhaul and limited life components from military aircraft. Computer programs were prepared under the M & R Program to list and analyze the reason-for-removal file and the parts-replaced and assemblies-scrapped file. A small computer program was prepared under this contract to correlate the reasons-for-removal and the reasons-for-scrappage by serial number of the blades scrapped by BHC.

4. Red River Army Depot (RRAD) Main Rotor Blade Inspection Records

These data initially contained the date of inspection, the blade part number and serial number, whether the blade was scrapped, to be held for additional records, or forwarded to a repair facility, and if scrapped, the reason for scrappage. Later the records were expanded to include the total time on each blade. Copies of these records were obtained by the BHC Quality Department as informal data exchange. The data on the records were transcribed into the OSM-634 tape files for listing and analysis using the existing overhaul data computer programs.

Flight hour data were obtained from two sources:

- Monthly flight reports of the M & R Program monitored aircraft
- Form DA1352 listings of flying hour data on BHC helicopters (Reference 1)

B. COMBAT AND NONCOMBAT AIRCRAFT

The combat aircraft were those stationed in Southeast Asia. All others were considered noncombat aircraft. The two data sources from which Vietnam aircraft or organizations could be identified were the TAERS 2410 data and the FDRs. They could not be determined from the BHC and RRAD data.

1. TAERS Data

BHC has 45 magnetic tapes of DA2410 data. To facilitate the analysis, two tape files were created, one of UH-1D/H blades (P/N 204-011-250-5) and one of UH-1C/AH-1G blades (P/N 540-011-001-5). Each blade record contains a code which identifies the organization that prepared the report. Insofar as possible, the codes in the blade file were identified using the Directory and Station List of the United States Army (Reference 2). The results are shown in Table VI.

TABLE VI. ORGANIZATION CODES IDENTIFIED IN TAERS DATA

	Blade	File
	UH-1D/ UH-1H	UH-1C/ AH-1G
Number of Army Codes In the Data File	237	164
Number Identified For Vietnam	164	120
Number Identified For CONUS	24	14
Number Not Identified	49	30

The existing computer program used to select the data (for example, the organizations coded in the removal records) was so designed that the number of different selection choices had to be limited to keep the computer time reasonable. The selection procedure limited the

choices to fifty organizations. Since less than fifty organizations other than those in Southeast Asia reported blade removals, the selection limitation did not affect the noncombat aircraft blades. However, 166 UH-1D/H and 122 UH-1C/AH-1G organizations in Southeast Asia reported blade removals, so fifty organizations in Vietnam were selected from each file. The organizations selected reported 7484 (77.5%) of the UH-1D/H and 2209 (76.4%) of the UH-1C/AH-1G blades removed in Southeast Asia which is an adequate sample.

All but fifty-six UH-1D/H and twenty-one UH-1C/AH-1G noncombat blade-removal records were from CONUS organizations so only CONUS organizations were used for the noncombat Two of the CONUS organizations' aircraft blade analysis. data were omitted because it was suspected that their blade removals were primarily from Vietnam aircraft sent back for These were Red River Army Depot and the U. S. Army repair. Aeronautical Depot Maintenance Center (ARADMAC). deletion reduced the number of CONUS removals by 2340 records (76%) for the UH-1D/H and 625 records (85%) for the UH-1C/AH-1G blades. From the above, four analysis files were established, two for each blade type for each of the two locations. To assure that only the improved blade removals were analyzed, all UH-ID/H blades records with serial number.: less than A2-2400 were eliminated.

If more time had been available, it may have been possible to salvage some of the ARADMAC removal records for the CONUS analysis. This would require identifying the serial numbers of the aircraft from which the blades were removed and with additional research determining the aircraft that were previously at a CONUS facility. Even so, it is probable that most of the reasons for removal were to facilitate maintenance.

2. FDR Data

The FDR data used in the MTBR analyses were those reports from the M & R Program field monitoring periods of:

- April 1966 through October 1967 for the UH-1C
- April 1966 through November 1967 for the FY 1965 and 1966 UH-1D/H
- July 1967 through October 1969 for the AH-1G

The CONUS and Vietnam data were analyzed separately. However, the UH-1D/H data for CONUS were inadequate

(0 removals) for the very small monitoring period (5851 flight hours) to provide any meaningful numbers.

C. REASONS FOR BLADE REMOVAL AND SCRAPPAGE

The reasons for blade removal were divided into four major classes (which are defined in Appendix A):

- Part Causes
- External Causes
- No Failure Causes
- Unknown Causes

These were further divided into subgroups as shown on Table VII. The individual removal reasons coded on TAERS data and reported in the OSM-634 files were assigned to the subgroup to which they seemed most appropriate. Reasons that did not seem to be appropriate blade failure modes or removal reasons were grouped with the "Unknown Causes." The individual removal reasons are shown in Appendix B.

The same major classes and subgroups were used to group failure modes found in the FDR data for the MTBR analyses.

The reasons for scrappage were also grouped into four major classes:

- Part Causes
- External Causes
- No Failure Causes
- Other Causes

These were further divided into subgroups as shown on Table VIII. The individual reasons for scrappage were placed in the subgroups that seemed most appropriate. The individual reasons for scrappage are shown in Appendix B.

While the BHC blade repair and scrap records contain the reason-for-removal that was reported on the DA2410 form received with the blade as well as the reason for scrappage, the RRAD records contained only the reasons for

TABLE VII. THE SUBGROUPS OF THE MAJOR REASONS FOR REMOVAL

I. PART CAUSES

- A. Excessive Vibration
- B. Deterioration
- C. Bonding Failure
- D. Excessive Wear
- E. Corrosion
- F. Other

II. EXTERNAL CAUSES

- A. Foreign Object Damage
- B. Overstressed
- C. Heat Damage
- D. Maintenance and Shipping Damage
- E. Other

III. NO FAILURE CAUSES

- A. Time Change
- B. Other

IV. UNKNOWN CAUSES

TABLE VIII. REASONS FOR SCRAPPAGE SUBGROUPS

I. PART CAUSES

- A. Imbalance
- B. Deterioration
- C. Bonding Failure
- D. Corrosion
- E. Water Contamination

II. EXTERNAL CAUSES

- A. Foreign Object Damage
- B. Overstressed

III. NO FAILURE CAUSES

- A. Time Change
- IV. OTHER CAUSES
 - A. Unknown

scrappage. In the past, as the RRAD data were received. assumptions were made as to the reasons for removal based on the reasons for scrappage, and these assumptions were entered into the data form when the RRAD were transcribed into OSM-634 format. Where an assumption could not be made the reason for removal was coded "Unknown." The RRAD data Reason for Removal/MTR analyses contained in Appendix F include the assumed removal reasons. However, when analyses were made to compare reasons-for-renoval with reasons-forscrappage, only the BHC data were used. Prior to the blades reaching a repair facility the reason-for-scrappage of a blade has been assumed to be the same as the reason-forremoval. (Exceptions to this assumption are the blades that are damaged during or after removal.) This assumption has been necessary because TAERS DA2410 data that BHC has received contain very few records of blade scrappage. even though there is a standard procedure for reporting scrapped serial-numbered items.

D. MEAN-TIME-TO-REMOVAL (MTR)

MTR for the main rotor blades is the sum of the times at removal for all blades divided by the number of blades removed.

$$\sum_{i=n}^{i=n} t_i$$

$$MTR = \frac{i=1}{n}$$
(1)

where

ti = the total time at removal of the ith blade,
 in hours

n = the number of blades removed

MTR was computed from TAERS, OSM-634 and RRAD data because these sources were the most adequate for this calculation. The blade removals that were for "no failure causes" other than "time change" were omitted from the TAERS data analysis. Since these removals were made to facilitate maintenance or to provide blades for another aircraft (cannibalization), etc., they are outside the scope of the snalysis. However, these reasons were included in the OSM-634 and RRAD data since the blades received for repair that were removed for these reasons were either damaged in the removal process or after being removed, or they were shipped to be repaired for another reason (perhaps unintentionally).

The unknown (or unstated) removal reasons were analyzed as a group. This was done to see whether the MTR for this group was similar to that obtained from the part and external cause removal records. A similar MTR would indicate the probability that the distribution of the "Unknown" group is similar to the combined part and external cause groups.

E. MEAN-TIME-BETWEEN-REMOVALS (MTBR)

The MTBR for main rotor blades is twice the sum of the flight hours of the group of aircraft from which the blades were removed divided by the number of blades removed during those flight hours.

$$2 \sum_{j=1}^{j=m} t_{j}$$
MTBR = $\frac{j=1}{n}$ (2)

where

t; = the total flight hours of the jth aircraft

m = the number of aircraft in the group

n = the number of blades removed

MTBR was computed from TAERS and FDR data because flight time for the aircraft were available for use with these sources.

1. MTBR From TAERS Data

To compute MTBR from TAERS data it was first necessary to select a group of aircraft for which total flight times could be established. Next the TAERS data were searched to identify every blade removal recorded against each of the aircraft. Each removal reason and blade time was recorded.

The aircraft selected were the same M & R Program monitored aircraft that were used to compute the MTBR from FDR data. This was done because these aircraft could be readily identified as to CONUS or Vietnam location. The main difference is the TAERS data cover the entire life of the aircraft through 31 December 1969.

MTR and reason-for-removal values for the total files (Vietnam and CONUS) were compared with the values calculated for the selected aircraft samples. The results (Appendix D. Table D-X) are similar for the UH-1C/AH-1G aircraft in Vietnam. There was less similarity between the values for UH-1D/H in Vietnam and very little similarity between the values for the UH-1D/H in CONUS. However, in the latter case there were only sixteen blade removals recorded in TAFRS for the ten monitored UH-1D/H's in CONUS, an inadequate sample for comparison.

No comparison could be made for the UH-1C/AH-1G CONUS because there were no CONUS removals recorded where other data did not show the aircraft also stationed in Vietnam.

2. MTBR From FDR Data

The FDR data were reviewed for the main rotor blade failures reported and those found were grouped into three sets:

- Failures that resulted in blade replacement
- Failures that resulted in blade removal for repair or replacement
- Failures that resulted in blade repair (either with blade removed or not removed) or replacement:

The first set is a subset of the second which is a subset of the third as shown in Figure 1.

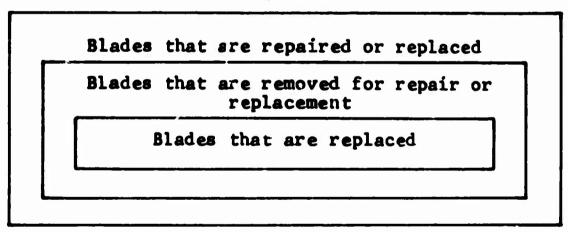


Figure 1. Set/Subset Relationship of the M/R Blade Failures Found in the FDR Data.

The results of this analysis are shown in Appendix E.

The MTBR values were computed for main rotor blade failures that resulted in the blade being removed for repair or replacement. The time base for the analysis was the sum of the flight nours for the aircraft during the monitoring period. The results are shown on Tables XII and XIII in Section IV together with the values obtained from TAERS data.

F. PROBABILITY OF SCRAPPAGE/REPAIR ANALYSES

Since the scrap probability analyses needed input from all three data sources, sample groups of data were selected from TAERS that had dates of removals for blades that would be expected to be found in the RRAD and BHC records. The data groups selected were those with Julian dates starting 72, 73, 80 and 81. Since this analysis could not be mechanized but required a serial number by serial number search through listings from each of the data files, only enough data groups were used to provide an adequate data sample. For the UH-1D/H blades, the single group of removals, Julian dates from 7200 through 7299, provided a sample of 331 blades. To obtain a comparable sample (336) of UH-1C/AH-1G blades, three date groups were required. from 7200 through 8099. After the date groups were selected, each blade serial number was researched through the TAERS data, the BHC repair/scrap records, and the RRAD scrap, forward, or hold records to determine whether the blade after removal for a part or external cause was reinstalled on another aircraft, forwarded to a repair center, scrapped, repaired, held, or again forwarded.

The results of this research were summed and percentages established. Based on the number removed and the number scrapped or repaired, a 90-percent confidence interval for the probability of scrappage or repair was computed. The confidence intervals were computed using the table and equations of Reference 3.

G. AIRCRAFT MAIN ROTOR BLADE SUPPORT COST ANALYSIS

Having already determined the percentage of blades that are removed for each cause and the percentage of the blades that are removed for part and external causes (premature removals) that are repaired by the using organization and by a blade repair facility, the blade support cost can be computed.

1. General

The aircraft main rotor blade support costs are a function of the following elements that are used in this analysis:

- The aircraft life cycle
- The rotor blade mean-time-to-removal
- The cost of blade removal and installation
- The cost of the blade repair system divided among the blades repaired
- The cost of a new blade
- The allowable operating (fatigue) life of a new blade
- The remaining life of a repaired blade
- The shipping costs of new and facility-repaired blades to the user

There are other costs involved in the aircraft blade support cost cycle that have been omitted from this analysis because they are not readily obtainable and because they are minor. Some of these costs include:

- Cost of inspection and scrappage by the using organization
- Cost of shipment from one CONUS location to another to finally arrive at a repair facility
- Cost of shipping containers for the blades. (These are reuseable)
- Cost of preparing removed blades for shipment
- Cost of inspection of blades scrapped at an inspection location (such as RRAD) in the return path to a repair facility
- Cost of repair materials at the user's location

The costs used have been put into three adjusted blade cost groups and the cost of shipping a repaired or new blade to the user. The three adjusted blade cost groups are:

- The cost of blades repaired by the user. This includes the cost of removal, repair and reinstallation of the blades repaired at his location.
- The cost of blades repaired by a repair facility. This includes cost of removal and installation of the repaired blade, the transportation cost of all the blades that are shipped back for repair, and the repair cost.
- The cost of a new blade is increased to include the cost of removal and installation.

The cost of the new blades originally installed on the aircraft is not included in the support cost analysis.

2. User Repaired Blade Cost

The following equation is used to compute this value.

$$C_{o_r} = \left(T_{r_1} + T_{r_2} + T_i\right) C_m \tag{3}$$

where

C_o = The dollar cost of repair of a removed blade by the using organization

T_r = The time in manhours to remove a blade asaembly

T_{r2} = The time in manhours to repair a blade at the removal area

T_i = The time in manhours to install the blade assembly

C_m = The manhour cost of organizational maintenance personnel

3. Facility Repaired Blade Cost

The cost of a facility repaired blade is computed using the following equation:

$$C_{r_{b}} = \frac{bC_{m}(T_{r_{1}} + T_{i}) + C_{s_{a}}(d) + C_{s_{s}}(1-d) + bC_{t_{r_{s}}}}{b}$$
(4)

where

C = The cost of a repair of blades shipped to
b CONUS for repair, dollars per blade
repaired

C_s = The dollar cost of shipping a blade to CONUS using air transportation

C_s = The dollar cost of shipping a blade to CONUS using surface transportation

C_t = The dollar cost of repairing a prematurely removed blade

b = The fraction of the blades shipped to CONUS for repair that are repaired

d = The fraction of the blades shipped to CONUS by air transportation

The remaining symbols are the same as those used for equation (3).

4. New Blade Cost

For this analysis, the new blade cost is adjusted to include the cost of removing the blade that was scrapped and installing the new one. This cost is computed using equation (5).

$$C_{n_b} = C_m \left(T_{r_1} + T_i \right) + C_{n_{b_f}}$$
 (5)

where:

 C_n = The adjusted cost of a new blade.

C_n = The cost of the new blade at the factory.

5. Blade Support Cost Analysis

The blade support cost is computed using the following equation:

$$C_{ts} = \frac{\left(\frac{nL}{MTR} - n\right)}{100L} \left(C_{n_b} \times g + C_{r_b} \times h + C_{s_a} \times e(g + h)\right)$$

$$+ C_{s_s} \times f(g + h) + C_{o_r} \times j$$
(6)

where

C_{bs} = Blade support cost in dollars per flight hour

L = Aircraft life cycle in flight hours

MTR = The mean-time-to-removal for repair or replacement in blade hours

g = The percentage of removed blades replaced
by new blades

h = The percentage of removed blades replaced by CONUS facility repaired blades

j = The percentage of the blades removed that are repaired by the using organization

e = The fraction of the blades shipped from CONUS that are transported by air

f = The fraction of the blades shipped from CONUS by surface transportation

n = The number of blades in the rotor

For these analyses

$$g + h + j = 100$$
 (7)

and

$$e + f = 1 \tag{8}$$

To compute the cost of repair by the using organization, the average blade removal, repair, and installation manhours

spent by the using organization were taken from a DA2407 Maintenance Report data listing for the UH-1H and AH-1G. The results are shown in Table IX.

TABLE IX. ORGANIZATIONAL MAINTENANCE MANHOUR REQUIREMENTS AND COSTS*

	UH	-1H	AH-	lG
Activity	Average Manhours	Dollars	Average Manhours	Dollars
Blade Removal (Tr1)	3.73	13.06	3.72	13.02
Blade Installation (Ti)	3.73	13.06	3.72	13.02
Blade Repair (Tr2)	6.00	21.00	6.50	22.75
TOTAL (Cor)	13.46	47.12	13.94	48.79

^{*} Costs are based on \$3.50 per organizational maintenance manhour. This is approximately a 30-percent increase over the \$2.67 shown in U. S. Army Field Manual 101-20 dated 15 December 1966 (Reference 4)

Cost of main rotor blade shipment to or from Southeast Asia is (Reference 5):

- \$114.00 by air transportation
- \$82.00 by surface transporation

Cost of a new blade at Bell Helicopter Company is (Reference 6):

- \$2918.19 UH-1D/UH-1H
- \$3151.71 UH-1C/AH-1G

The average cost of blade repair at Bell Helicopter Company (as developed by the Cost Analysis Group) is:

- \$925.00 UH-1D/UH-1H
- \$787.00 UH-1C/AH-1G

The allowable operating time (AOT) for the blades is (References 7, 8, and 9):

- 2500 hours UH-1D/UH-1H
- 1100 hours UH-1C/AH-1G

From the earlier analyses, the MTR's of the blades removed in Vietnam and of the blades repaired at BHC, the ratio of the fatigue life remaining in the repaired blade to the blade MTR was developed as shown in Table X.

TABLE X. LIFE REMAINING IN REPAIRED BLADES

	Bla	ades
	UH-1D/H	UH-1C/AH-1G
MTR of blades removed in Vietnam	409 hrs	316 hrs
MTR of blades repaired at BHC	310 hrs	241 hrs
Blade AOT	2500 hrs	1100 hrs
Fatigue life remaining in BHC repaired blades	2190 hrs	859 hrs
Ratio of the fatigue life remaining to the MTR of blades removed in Vietnam	5.4:1	2.7:1

Since the ratio of the fatigue life remaining on the repaired blade to the Vietnam blade MTR is high, the analysis does not include the consideration of the reduced life of the repaired blades.

IV. ANALYSIS RESULTS

A. MTR ANALYSIS

1. Model UH-1D/UH-14 Blades

Table XI from TAERS data shows that the All Data values closely resemble the Vietnam data values. This is to be expected since the majority of the blade removal records were from aircraft stationed in Vietnam. The CUNUS values are considerably higher than those from Vietnam. Also a much higher percentage of CONUS blades survive to scheduled retirement life. This reflects the difference in environment vulnerability of the blade to the two use locations. The combat environment produces blade strike and foreign object damage (FOD) (i.e., bullet damage). Also, the maintenance care given to the blades in CONUS is a ricety that must be of a lower priority in the combat zone maintenance environment.

The percentage of the blades removed for "External Causes" in Vietnam is almost three times that for "Part Causes." In CONUS, the percentage removed is less for "External Causes" than for "Part Causes." A review of the more detailed tables in Appendix D shows that the major external removal cause in Vietnam is the combination of "battle damage" and "punctured" (almost 1000 removals) which is practically nonexistent in the CONUS data (four removals).

2. Model UH-1C/AH-1G Blades

Table XII shows characteristics very similar to those of Table XI for the UH-1D/H blades. The MTR values are somewhat lower than those for the D/H blades. The percentage for "External Cause" removals in Vietnam is again almost three times the percentage of "Part Cause" removals, with "battle damage" and "punctured" again being the major external removal cause. The CONUS MTR values had to be determined from a very small number of removals. At the end of March 1970, Bell Helicopter Company helicopter operation records show that over 47 UH-1C and 79 AH-1G aircraft were assigned to CONUS organizations (not including aircraft being rebuilt at ARADMAC and the BHC Amarillo facility or recently delivered aircraft in transit). These numbers of aircraft are small when compared to the number stationed in Vietnam, and either only a few have had blade removals, or, what is more likely, all the removals are not being reported. Even so, it is significant that a comparitively large percentage of the CONUS blades is replaced for time change.

TABLE XI. REASONS FOR REMOVAL AND MEAN-TIME-TO-REMOVAL (UH-1D/H MAIN ROTOR BLADES)

Blades From Aircraft Model(s): UH-1D/H					Part No.: 25m-1250-5	A-1.:-256-5
	VIT DIL	DATA	VIETNAM DATA	H DATA	CONTS SATA	27.25
REASON FOR REMOVAL	MTR	PERCENT OF ALL CAUSES	XIX	PERCENT OF ALL CAUSES	K.	PRIENT OF ALL
ALL CAUSES	453.5	100.00	9.907	100.00	593	8.
I. PART CAUSES	2.948	26.04	5.9.5	239	330.5	
A. Excessive Vibration	355.1	6.34	396.5	÷. 96	\$32.2	
B. Deterioration	597.3	67.00	538.6	* : : 6		
C. Bonding Failure	580.8	5.80	5.5.5	56	9-69.3	:
D. Excessive Wear	657.4	3.64	594.2	3.84	. 356.	
E. Corrosion	6.849	1.57	557.5	38:1	\$35.3	•
II. EXTERNAL CAUSES	398.8	63.10	369.4	50	• 59.	
A. Foreign Object Damage	398.5	53.82	373.3	5e.76	3 43	
B. Overstressed	† · 00 †	9.02	348.5	:0.03		
	349.7	0.18	333.1		•	
D. Maintenance and Slipping Damage	106.0	10.0	•	00 0	•	3
E. Other	583.6	0.06	179.5	0.09	•	
III. NO FAILURE CAUSES	1,658.8	30.1	5.5%	0.35	1.50	
A. Time Change	1,658.8	30.1	3.676	0.35	36	:
IV. UNKNOWN CAUSES	428.4	08.6	7.63.	: 7.	2007	9
TOTAL NO. OF REMOVALS	8.222	22	6097	60		333

* Does not include Red River Army Depot and ARADMAC coded blade removals.

TABLE XII. REASONS FOR REMOVAL :NO MEAN-TIME-TO-REMOVAL (UH-1C/AH-1G MAIN ROTOR BLADES)

Blades From Aircraft Model(s): UM-1C/AM-1G					Part No.: 54	\$40-011-001-8
	VIT DVIV	ATA	VIETIMH DATA	DATA	COMUS DATA	DATA.
REASON FOR REDOWL	KIR	PECENT OF ALL CAUSES	E.	PEACENT OF ALL CAUSES	Ę	PERCENT OF ALL
STIN CAUSES	337.7	100.00	₹"51€	100.00	-75.7	30.00
I. PART CAUSES	9"142	36.14	371.1	23.45	÷55.3	3.3
A. Excessive Vibration	258.5	3.2	324.6	6.68	208	15.09
1. Deterioration	393.7	6.72	410.9	99.9	į	9.43
C. Bonding Pailura	9.14	5.35	340.3	5.43	97.0	3.77
D. Excessive Wear	412.4	2.72	418.3	3.03	372.0	-1
E. Corresion	427.5	1.41	412.7	2.63	262.0	58:
II. EXTERMAL CAUSES	283.6	\$6.49	271.7	68.79	290.2	.5.
A. Foreign Object Danage	205.4	95.40	279.7	58.70	232.0	30
B. Overstressed	273.1	9.17	223.6	9.30	7:3	32
C. Neat Damage	201.0	0.27	117.7	0.23	•	0.8
D. Maintenance and Shipping Damage	468.5	60.0	488.5	9::0	•	0.00
III. NO PALURE CAUSES	205.7	92.4	3.46	2.33	350.7	19.63
A. Time Change	985.7	4.76	924.1	2.33		:9.6:
IV. MICHOLI CAUSES	2.005	21.9	265.2	5.43	2.9.3	3.66
TOTAL NO. OF REDVALS	3.	2.20%	1	1,288		

* Does not include Red River Army Depot and APADIMC coded blaza removals.

B. MTBR ANALYSIS

1. Model UH-1D 'UH-1H Blades

Table XIII shows fairly similar results from the two data sources for the Vietnam blades. The CONUS values are questionable since the time base is so low. The main difficulty with this analysis was that aircraft had to be selected that were stationed for the majority of their life in either Vietnam or CONUS. It was fairly easy to identify aircraft for the Vietnam analysis, but there were very few CONUS aircraft that could be identified that had not spent a good portion of their operating life in Vietnam.

It is interesting to note that the Vietnam results show that the MTBR for "external cause" removals is about one-third that for "part cause." This means the removal rate for "external cause" removals is again about three times that for "part cause," which is in agreement with the results of the MTR analysis.

2. Model UH-1C/AH-1G Blades

Table XIV shows marked similarity of Vietnam MTBR values for the two data sources. It also shows the three-to-one removal rate relationship between the "external cause" and "part cause" removals.

The TAERS CONUS data records were too few to provide a meaningful analysis. The M & R CONUS analysis shows the higher mean-times that can be expected from the better use environment.

C. MAIN ROTOR BLADE SCRAP ANALYSIS

1. General

Through the UH-1/AH-1 M & R Program and other sources, it was determined that the following are the basic reasons that a blade removed from an aircraft is scrapped:

- The blade has achieved its allowable operating time.
- The blade is damaged beyond repair prior to removal.
- The blade is damaged beyond repair during or after removal.

TABLE XIII. REASONS FOR REMOVAL VERSUS MEAN-TIME-BETWEEN-REMOVALS (UH-1D/H MAIN ROTOR BLADES)

Blades From Aircraft Model(s): UM-1D/M			Parr No.	Far: No. 204-01250-5
		MEAN TIDE BETWEEN AENCHALS	EEN AENCHALS	
	HYKLIIA	NW.	SINO	C.S
TOTAL METADORIT	VIVO VIVO	TAERS	vive vive	SATIS SATIS
AL CAUSES	416	:,063		333
I. PART CAUSES	\$77.5	5,540		
A. Excessive Vibration	22.600	72.279		3.839
B. Deterioration	•	.0.070	0)	•
C. Bonding Pailure	6.460	9.637	• 3	•
D. Excessive Wear	•	144.556	n To	•
E. Corresion	•	•	ra No p	•
II. EXTERNAL CAUSES	1,211	1.326		. 4 . 2
A. Foreign Object Demage	1.948	1.4:7	ار و ارون	
B. Overstressed	3.200	20.65.	# 3 i	•
C. Heat Damge	•	•	riefą,	٠
D. Maintenance and Shipping Damage	•	•	fo .e	•
III. NO PAILURE CAUSES	.			3.6.
A. Time Change	•	•		
IV. UNCHOLM CAUSES		355' 777.		-
Blade time base, hours	64.800	344.556	4324	3.8

TABLE XIV. REASONS FOR REMOVAL VERSUS MEAN-TIME-BETWEEN-REMOVALS (UH-1C/AH-1G MLIN ROTOR BLADES)

Blades From Aircraft Model(s): UN-1C/AM-1G			Part X	Part No.: 546-01:-001-5
		HEAK TINE B	HEAN TIDE BETVEEN RENOVALS	
BEAGON POD DEPONAL	×	VIETWAN	ö	CONUS
	PAR	TABAS	MER	TAERS
ALL CAUSES	930	908	1,449	
I. PART CAUSES	4,067	3,602	2.974	
A. Excessive Vibration	16,392	11.346	6.279	e n j
B. Deterioration	16,733	11.943	86.50	FA
C. Bonding Pailure	10,928	13.348	8.073	••
D. Excessive Wear	26,226	75,640	28.254	out
E. Corrosion		56,730	•	۱.
II. EXTERIAL CAUSES	1.203	1.252	4.036	2nd
A. Foreign Object Damage	2.017	1.609	1	wn.
B. Overstrassed	6.5%	5.972	5.65	. 0
C. Heat Demage	•			•
D. Maintenance and Shipping Demage	196.5	113.640	\$6.508	1
E. Other	65.366	•	•	a, ctr
III. NO PALLURE CAUSES	-	56,730	14,127	p#u
A. Time Change	•	56,730	14.127	, .
IV. UNIQUOM CAUSES	-	113.460	28,254	<u>.</u> L
Blade time base, hours	131.132	226.920	\$6.508	!
				- W

- The blade, reparable when removed, is improperly handled and packaged after removal and deteriorates beyond repair.
- The blade, thought reparable when removed, is later found to be either too badly damaged or too badly deteriorated to repair.
- The blade has too little fatigue life remaining to make facility repair economical.
- The time records for the blade are lost, and its appearance indicates that it might be dangerous to repair it and assign a time value.

Because most of the blades that were scrapped were not identified in TAERS, it was necessary to make certain assumptions concerning the TAERS data records that show that a blade was removed for part or external causes. They are:

- If there are records that show that the blade was later either installed on or removed from an aircraft, then the blade had been repaired after its original removal.
- If there are codes in the records that show that the blade was shipped to a repair facility, then it is assumed that the blade was shipped after removal and was not repaired by the organization that did the removal.
- If there are no records from any source on the blade after removal then it is assumed that it was scrapped by the organization that did the removal.

The Red River Army Depot (RRAD) was a receiving point for main rotor blades returning to CONUS for repair. Until recently, RRAD inspected the incoming blades and scrapped those that were not economically reparable, based on their inspection criteria. The remainder were either forwarded to a repair facility or held pending the receipt of adequate records. Since RRAD's inspection of the blades was limited to what could be seen without disassembly, most of their reasons for scrappage were for external causes. The initial RRAD data were obtained in

September 1967. Later in 1968, the total time on the blades was also included in the data. The RRAD log sheets were received until 26 May 1969, about the same time as the end of BHC's then-current blade-repair contract.

The scrap probability analyses needed input from all three data sources. Sample groups of TAERS data were selected that had dates of removal for blades that would be expected to be found in the RRAD and BHC records. The data selected were those with Julian dates starting 72, 73, 80 and 81. A review of these data showed that the number of CONUS part and external cause removals was too small and was therefore inadequate to obtain meaningful analysis values. For this reason, the probability analyses were conducted using only Vietnam blade removal records.

2. Probability of Scrappage and Repair

Tables XV, XVI, XVII, and XVIII, which summarize the results of the probability of scrappage and probability of repair analysis, show a somewhat different ratio of externally caused removals to part caused removals from that seen in the previous tables. Instead of the three-to-one ratio, the ratio is a little over two to one for the UH-1D/H blades and a little over six and one-half to one for the UH-1C/AH-1G blades. This indicates that the blade removal distributions for the periods used in the scrappage analysis were not typical of the total Vietnam blade removal distributions. This shows the need for further study. For example, the "external cause" to "part cause" removal ratio may increase considerably when other time periods of data are analyzed. This increase could relate to periods of intense battle activity such as the TET offensive in January - February 1968, when inspection criteria, the rate of field repairs, and the percentage of blades scrapped by the removing organization was extremely different from the average or normal situation.

Although the percent scrapped is similar for the two blades for combined causes, the percentages differ considerably between the two-blade types for some of the subclasses of removal reasons. For example, over 90 percent of the D/H blades removed as "overstressed" were scrapped, while only 59 percent of the C/G blades removed for the same reason were scrapped. Conversely, over 94 percent of the C/G blades removed for "deterioration" were scrapped, while only 56 percent of the D/H blades removed for this reason were scrapped. Although this variance was not explained by the analyses conducted, it is probably partially

TABLE XV. PROBABILITY OF SCRAPPAGE OF UH-1D/H MAIN ROTOR BLADES REMOVED IN VIETNAM

Blades From Aircraft Model(s): UH-LD/H	del(s):	UH-10/H								Part No.	Part No. 204-011-250-5
		Removi	Removing Organizacion	14th on		Inspec	1 on/ Repair	Inspection/Repair Facility		Total	
á			Scrapped	Scrapped Probability			Scrapped	Scrapsed Probability		Seraphed	1.0
for Removal	Total	No. Scrapped	Total Removed	Confidence Interval)	Total	Serapped	Toral Snipped	Confidence Interal	No. Scrapped	CC. S. Recver	Cont. dence
COMPLINED CAUSES	337	\$61	7746	27.7 - 35.1	197	77		27.7 - 27.2	<u> </u>	:1	12 4.8.
I. PART CAUSES	ट्य	ন	70.4	14.7 - 27.6	55	S	53	54.5 - 23.7	4	3.60	9 38 - 35
A. Excessive Vibration	77	a	23.5	3.5 - 46.1	Ť	۰	56.7	34.5 - 90.2	<u> </u>	. 82 . F	36.4 - 78.5
S. Deterioration	32	^	21.9	12.3 - 35.8	12	::	52.4	32.2 - 72.4	. d	2.45	9 - 5 - 7
C. Bonding Failure	32	۰	18.7	10.0 - 32.4	3,	16	26.4	-7.9 - 52.2	C4 C1		54.3 - 56.3
D. Excessive Wear	17	n	17.6	5.0 - 39.0	ø,	•	8.7.8	51.9 - 49.m	:	4. e.	35.4 . ***
E. Corrosion	5	1	20.0	1.0 - 65.7	Ö	•	•	٠	.4	;;	
II. FYTERIAL CAUSES	\$27	킕	8.95	31.8 - 42.2	इटा	6	64	6.3 6.56	:1		
A. Foreign Object Denege	506	76	36.9	31.6 - 42.6	111	7.5	67.4	+. n - 6. 65	·:	;; ;;	58.0 - 5.3
B. Overstressed	22	•	36.4	19.6 - 56.1	14	21	55.7	bl.5 - 9"."	20	30.0	1.95

*Part Causes and External Causes Only

TABLE XVI. PROBABILITY OF SCRAPPAGE OF UH-1C/AH-1G MAIN ROTOR BLADES REMOVED IN VIETNAM

Blades From Aircraft Model(s): UH-1C/AH-1G	aft Mode	1(s): UH	1-1C/AH-1G							Par	Part No. 540-011-001-5	11-001-5
			Remov i	Removing Organiz	nization		Inspect	Inspection/Repair Facility	Facility		Total	
8		 _		Scrapped	Scrap Probability (90%			Scrapped	Scrap Probability		Scrapped	Scrap Probability
for Removal		Total Removed	No. Scrapped	Total Removed	Confidence Interval)	Total Shipped	No. Scrapped	Total Shipped); []	No. Scrapped	Total Removed	Confidence Interval)
COMBINED CAUSES		336	791	2.42	9.82 - 7.64	001	22	72.9	5.8 5.49	न्दर	75.6	73.5 - 79.2
1. PART CAUSES	1924	73	73	52.3	40.1 - 64.2	77	위	41	9.68 - 0.94	33	25.0	53.0 - 84.1
A. Excessive Vibration	* 8	11	v	45.5	20.0 - 72.9	m	, a	33.3	1.7 - 86.5	्रक	¥:	27.1 - 80.0
B. Deterioration	ration	18	13	72.2	50.2 - 88.4	s	3	80.0	34.3 - 99.0	17	1.46	76.2 - 99.7
C. Bonding Failure		^	3	57.1	22.5 - 87.1	7	۲,	100.0	22.4 -100.0	ø	65.7	47.9 - 99.3
D. Excessive Wear	ve Wear	2	0	0.0	0.0 - 28.0	4	e	75.0	24.9 - 98.7	n	42.9	12.9 - 77.5
E. Corrosion	uo	1	1	100.0	10.0 -100.0	0	ı	•	•	~	100.0	10.0 -100.0
II. EXTERNAL CAUSES	USES	262	द्धा	कृष्	7.65 - 9.67	36	79	1.27	63.6 - 79.3	777	3	73.3 - 79.6
A. Foreign Object Demage	Object	270	147	34.4	49.4 - 59.4	0	19	76.2	67.6 - 93.1	208	0,	72.6 - 61.0
B. Overstressed	Passa	22	12	\$4.5	35.3 - 72.9	9		16.7	0.9 - 58.2	£.;	59.3	39.5 - 76.7

*Part and External Causes Only

TABLE XVII. PROBABILITY OF REPAIR OF UH-1D/H MAIN ROTOR BLADES REMOVED IN VIETNAM

Blades From Aircraft Medel(s): UH-1D/H	Ddel(s): U	1-10/1							Par	Part Mc. 204-011-250-5	011-250-5
		Removi	Removing Organization	a tion		d w	Repair Facility	ty		Total	
			Periadag	Repair Probability			Repaired	Repair Probability		Repa: red	Repair Probability
for Been al	Total	No.	Total	Confidence Interval)	Total Shipped	No. Repaired	Total Shipped	*:	Nc. Repaired	Total Removed	Contidence Interval
-STEIN'S CALLESS	17.7	ম	न्त	9.2 - 15.0	791	श	1777	19.3 - 29.6	3	77.	2:02 - 20.5
1. PART CAUSES	কো	क्ष	नश	13.8 - 26.6	62	긔	22.5	:5.: - 32	시	33.0	0.64 - 9.33
A. Escessive Vibration	17		23.5	8.5 - 46.1	•	n	33.3	9.6 - 65.5			21.2 - 63.5
B. Deterioration	32		12.5	5.7 - 25.1	21	s	23.8	9.9 - 43.7	ď	1.62	17.2 - 42.5
C. Bonting	25	~	6.3	2.1 - 17.2	42	~	30.6	9.6 - 38.9		6.	9 · S · C · C · C · C · C · C · C · C · C
D. Excessive Wear	17	•	35.3	16.6 - 58.0	97	~	::.5	0.6 - 47.1			21.2 - 63.6
E. Corresion	\$	3	80.0	34.3 - 99.0	0	•	•	•		9 0.0	3-3 - 99.0
TIT DILDERY COURTS	777	গ	८. ८	8-41 - 8-5	527	33	8.45	19.0 - 31.6	35	6.15	3.35 - 36.6
A. Poreign Object Demage	20 6	13	9.5	6.4 - 13.1	111	30	27.0	20.7 - 34.4	?	23.8	36.3 - 29.0
B. Overstressed	22	0	0.0	0.0 - 9.9	22		7.1	0.4 - 29.3	•	.9	

Part and External Causes Only

TABLE XVIII. PROBABILITY OF REPAIR OF UH-1C/AH-1G MAIN ROTOR BLADES REMOVED IN VIETNAM

Stodes from Alteract Modelis): UN-IC/AN-IC	20 : CS \10	31-W/31-10							Par	Part No. Sec-011-561-5	-011-50:-5
		Removi	Removing Organiz	Lation		સ	Repair Facility	1:A	r)	Total	
Reson for	Total	ģ	Repaired of Total	>	Tot & !	. %	Repaired of or	Repair Probability () ()	Ÿ.	2 3 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	Repair Probatity (90%
Removal.	Regoved	Repaired	Removed		Sh: pped	Repaired	Shipped		Repa. red	Resoved	I. ers.
CONSTRETO CAUSES	अर	시	1 -91	13.0 - 19.6	0.51	तः	ें दर	* Ut - \$ 91	: 1	0	5-32 - m. 6.
1. PART CAUSES	3	7	स्र	9.9 - 26.9	귀	7	23.4	5.3 - 6.6	ं	33.7	11 - 35
A. facessive Vibration	11	r	27.3	7.9 - 56.4	•	~	56.7	13.5 - 99.3	so.	45.5	30.0 - 72.9
B. Deterioration	18	0	0.0	0.0 - 12.0	10	c	0.0	0.0	Ü	υ 0	0.0
C. Bonding Failure	^	-4	14.3	0.7 - 52.1	2	0	0.0	3.0 - 65.4			
D. Excessive Wear	^	n	42.9	12.9 - 77.5	.1	•	25.0	1.3 - 75.1	==		22.5
E. Corrosion	1	0	υ.υ	0.04 - 0.0	C	•	ı		0	O.	
II. EXTERNAL CAUSES	292	7.5	191	8-61 - 4-25	झ	1	1777	36.5 - 21.5	<u>ا</u> نا	544	
A. Foreign Object Demage	270	ſ3	.5.4	12.6 - 19.9	.	51	. S. B.	12.6 - 26.9	ŠŠ	÷.:	5.5
B. Overstressed	22		18.7	6.5 - 36.9	ý	\$	93.3	: . & - 8. : t	o	6.04	3: 3: - 60.5

*Part and External Causes Only

related to the conditions that prevailed suring the periods for which data were analyzed. With additional time, more data periods could be examined to determine if the variance is consistent. (Note that the large percentage (72%) of the C/G blades removed for "deterioration" were scrapped by the removing organization and that the period analyzed included the TET offensive of January-February 1968.) This variance precludes the establishment of special criteria for certain type removals; i.e., it would be in error to direct the scrappage of blades at the point of removal for overstress or deterioration.

It is interesting that while the removing organization scraps a higher percentage of the C/G blades (54.2%) than of the D/H blades (31.7%), it also repairs (or reuses) a higher percentage of the C/G blades (16.1%) than of the D/H blades (11.8%). Thus it naturally follows that a higher percentage of the D/H blades are shipped to CONUS for repair (56.6% versus 29.8% for the C/G blades). However, since about the same percentage of the blades shipped of each type are scrapped, this means that a higher percentage of the D/H blades that were removed are being scrapped after shipment to CONUS (38.4% versus 21.4% for the C/G blades). This suggests that better inspection criteria should be used by the organization removing the UH-1D/H blades in order to reduce the number of blades shipped to a repair facility that should have been scrapped. However, since the UH-ID/H data analyzed was only for a 100-day period in 1967, it may not be typical of later removal periods. Unfortunately, the authorized time remaining for this study when this characteristic was observed did not permit it to be investigated.

The percent scrapped plus the percent repaired do not add to 100 percent. This is because the final disposition could not be assumed for the blades held at RRAD for additional records or for the blades forwarded from RRAD to a repair facility from which there are no further data.

3. Reason for Removal Analysis of BHC and RRAD Blade Data

Tables XIX and XX show that although about the same percentage of D/H and C/G blades are scrapped, the percentage differs considerably for blades removed for part and external causes (and their subcauses). A lower percentage of C/G blades removed for part causes are scrapped than for the D/H blades similarly removed (45% versus 65.3%). Conversely, a higher percentage of the C/G blades removed

TABLE XIX. REASON FOR REMOVAL AND MEAN-TIME-TO-REMOVAL OF BLADES PROCESSED AT BHC AND RRAD**
(UH-1D/H)

:

Blades From Alfcraft Model(s): (M-LD/H						F No.:	204-0.1-250
	SICOES	BLADES PROCESSED.	BLADES	BLADES REPAIRED	BLADES	S SCHAPPED	\$30 83 40 \$430 834
REJSON FOR REMOVAL	MTR	PERCENT OF BLADES PROTESSED	ži.	PERCENT OF BLADES PROCESSED	č;	PERCENT OF BLACES PROCESSED	#3.025.52 T.A.T. AERE S.J.A.PRED -8Y. GAUSE
ALL CAUSES	429.3	100.0	310.0	33	1.14	7	
I. PART CAUSES	450.8	16.5	308.8	5.3	1.025	4.3	
A. Excessive Vibration	3:0.4	3.7	277.1		3	(m)	
5. Deterioration	449.7	3.6	274.9	11	533.3	.1	
. C. Bonding Failure	457.2	5.5	318.:	an .:	27	e i	
D. Excessive Wear	537.6	2.8	357.0	;	403.5		
E. Corrosion	0.602	0.7	395.7		4	3	1
F. Other	258.0	0.2	213.0	30.0	269.2		
II. EXTERNAL CAUSES	364.9	47.0	265.6	15.0		32.3	:
A. Foreign Object Danage	372.3	32.2	272.3	20:	6	2	
B. Overstressed	345.1	:3.8	246.6	6.4	34.4	9	1
C. Heat Demage	494.0	0.3	518.0	C.:	0.01-	• •	() () ()
D. Maintenance and Shipping Damage	379.5	6.0	277.5	0.3	4.8.4	, ;	
III. NO FAILURE CAUSES	\$05.7	1.1	7. 124	0.3	3:7.3		;
A. Time Change	2.064.6	0.3	•		2. 50.0	()	
B. Other	491.0	111	421.4	6.3	5.8.2	•	
IV. UNDOWN CAUSES	487.3	35.2	<u>5.5.0</u>	1777	\$55.2	33.5	

* Blades processed equals blades repaired at BHC plus those acrapped at BHC and at Red River Army Depot.

** Records with part time only

TABLE XX. REASON FOR REMOVAL AND MEAN-TIME-TO-REMOVAL OF BLADES PROCESSED AT BHC AND RRAD**
(UH-1C/AH-1G)

Blades From Aircraft Model(s): UM-1C/AH-1G						Part No.:	3-100-110-0-3
	BLADES	BLADES PROCESSED.	BLADES	BLADES REPAIRED	SECULE	BLADES SCRAPPED	PERCENT OF BUADES
REASON FOR REMOVAL	HTR	PERCENT OF BLADES PROCESSED	MTR	PERCENT OF BLADES PROCESSED	XIK	PERCENT OF BLADES PROCESSED	That Wase Schapped -BY CAUSE
ALL CAUSES	3.148	100.0	7.752	32.1	355.7	67.3	\$7.9
I. PART CAUSES	2.648	9.41	2.142	9.0	-9C.7	6.6	2.24
A. Excessive Vibration	323.4	8.0	240.6	5.1	6.564	5.5	32.4
B. Deterioration	321.2	3.0	195.9	1.5	4.544	· ·	\$0.0
C. Bonding Failure	351.9	2.3	209.6	6.0	-23.6	:	8
D. Excessive Wear	647.2	9.0	548.3	6.3	0.047	6 .0	\$0.0
E. Corrosion	502.0	0.7	•		502.0		30.001
II. EXTERNAL CAUSES	286.6	55.3	235.6	3.3	302.7	2	3.9
A. Foreign Object Damage	292.3	45.6	251.5	.:	366.0	•	36
B. Overstressed	268.5	9.6	230.5	\$.5	329.2	,/1 1	36.0
C. Heat Damage	•		•		•		
D. Maintenance and Shipping Damage	106.2	0.5	29.0	.0	4:5.0	::0	26.6
III. NO FAILURE CAUSES	9.118	7.9	306.0		0.916	::	\$2.5
A. Time Change	973.0	4.4	•		973.0	1	3
B. Other	397.9	1.8	306.0	::	550.2		47.18
IV. UNICHOFF: CAUSES	342.3	23.9	0.245	3.6	₹**!\$ *		5.43

* Slades Processed equals blades repaired at B4C plus those scrapped at B4C and at Red River Army Depot.

** Records with part time only

for external causes are scrapped than for the D/H blades similarly removed (76.0% versus 68.0%). The tables show that the MIR for the scrapped blades is considerably higher than that for the repaired blades (176.9 hours higher for the D/H blades and 147.3 hours higher for the C/G blades).

4. Reason for Scrappage Analysis of BHC and RRAD Blade

Tables XXI and XXII which compare the scrappage at RRAD and at BHC show that a much larger percentage of the C/G blades were scrapped at RRAD than were scrapped at BHC, while almost the same percentage of the D/H blades were scrapped at the two locations. In both blade groups between 80 and 90 percent of the blades scrapped at RRAD were scrapped for external causes.

5. Reason for Removal Versus Reason for Scrappage Analysis

From the previous analyses it was apparent that by the time the blades arrived at the repair facility most of the blades that were obviously unreparable were scrapped. The blades that are scrapped at the repair facility are blades with defects that are only discernable when disassempled or at least given a more detailed inspection than that normally achievable at the previous inspections. Therefore, in Table XXIII, it is not surprising that the majority of the reasons for the D/H blade scrappage at the repair facility (in this instance, BHC) are grouped under the part cause classification. It is surprising that in Table XXIV the same is not true for the C/G blades. Over three times as many D/H blades were scrapped at BHC for part cause than for external causes, while for the C/G blades the opposite was true at a ratio of 1.9 to one. The big factor in D/H blade scrappage was water contamination (44% of the blades scrapped), while for the same cause only a comparatively small percentage (6%) of the C/G blades were scrapped. This was so even though both were of the improved blade design. This implies that adding the improvements to the existing blade design (D/H) is not as effective as incorporating them in the original design as was done for the UH-1C/AH-1G blade.

D. AIRCRAFT MAIN ROTOR BLADE SUPPORT COST ANALYSIS

1. Blade Costs

The results of the adjusted blade cost computations are shown in Table XXV.

TABLE XXI. SUMMARY OF REASONS FOR SCRAPPAGE OF UH-1D/H MAIN ROTOR BLADES SCRAPPED BY BHC AND RRAD

Model UH-1D/H

Dwg /Part No. 204-011-250-005

	REASON FOR SCRAPPAGE	Percent	of Total	Scrapped
	REASON FOR SCRAPPAGE	RRAD	внс	TOTAL
ALL CAU	SES	50.57	49.43	100.00
I.	PART CAUSES	7.24	36.27	43.51
	A. Imbalance	0.00	.45	.45
	B. Deterioration	0.07	1.22	1.29
	C. Bonding Failure	0.52	2.82	3.34
	D. Corrosion	6.65	9.99	16.64
	E. Water Contamination	0.00	21.79	21.79
II.	EXTERNAL CAUSES	42.71	11.94	54.65
	A. Foreign Object Damage	33.38	7.07	40.45
	B. Overstressed	9.33	4.87	14.20
III.	NO FAILURE CAUSES	0.38	0.14	0.52
	A. Time Change	0.38	0.14	0.52
IV.	OTHER CAUSES	0.24	1.08	1.32
	A. Unknown	0.24	1.08	1.32
No	. of blades scrapped	1453	1420	2873

TABLE XXII. SUMMARY OF REASONS FOR SCRAPPAGE OF UH-1C/AH-1G MAIN ROTOR BLADES SCRAPPED BY BHC AND RRAD

Model: UH-1C/AH-1G Dwg /Part No. 540-011-001-005

	DEACON POD CODADDAGE	Percent	of Total	Scrapped
	REASON FOR SCRAPPAGE	RRAD	внс	TOTAL
ALL CAU	S ES	65.03	34.97	100.00
I.	PART CAUSES	1.85	10.46	12.31
	A. Imbalance	0.00	0.31	0.31
	B. Deterioration	0.00	2.26	2.26
	C. Bonding Failure	0.62	0.62	1.23
	D. Corrosion	1.23	5.13	6.36
	E. Water Contamination	0.00	2.15	2.15
II.	EXTERNAL CAUSES	57.44	19.90	77.33
	A. Foreign Object Damage	54.97	16.10	71.08
	B. Overstressed	2.46	3.79	6.26
III.	NO FAILURE CAUSES	5.44	2.05	7.49
	A. Time Change	5.44	2.05	7.49
IV.	OTHER CAUSES	0.31	2.56	2.87
	A. Unknown	0.31	2.56	2.87
No.	of blades scrapped	634	341	975

TABLE XXIII. SUMMARY OF REASONS FOR REMOVAL VERSUS REASONS FOR SCRAPPAGE OF UH-1D/H BLADES SCRAPPED AT BHC

1042 13 13 14 15 15 15 15 15 15 15	Blades from Aircraft Model(s): UH-1D/H				1	11		ELSON	SON FOR	SCAPPAZ	: L	5 5	No.: 204-11-256-5	
IL CANISTS 1920 1921 1922 1923 1924 1925 1				/,	Λ,	\mathcal{N}	1 63.	1 647.7		14.	1 3/	100	. N	
Table 1420 1642 15 16 18 18 18 18 18 18 18	REASON FOR REMOVAL	13		1334		1,44		a de la companya de l			135	\$ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	131	18/
Vibration 291 250 2 1 92 131 35 7 4 3 0 fon 68 53 - 3 10 33 7 4 3 10 33 7 4 3 0 1 6 10 33 10	3		2401		SI	L	185	\$29	Į.		[3]	1.		
Vibration 57 50 2 3 10 33 7 4 3 5 2 2 3 10 33 7 4 3 50 12 4 6 33 50 7 4 6 7	ART CAUSES	162	82	~	~1	31	22	111	5	ন	=	01	ام	
fon 68 53 - 3 25 22 12 6 7 3 6 7 3 6 7 3 6 6 6 7 3 6 6 6 6 7 3 6 6 6 6 6 6 6 6 6 6 6 6 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 2 2 2<	. Excessive Vibration	57	20	7	7	.	01	33	7		E	0	٠	
Mear 100 92 - 1 6 33 50 - 3 4 0 Mear 50 40 - 1 4 15 20 10 7 3 6 Mear 12 11 - - - - - 9 3 0 - - 0 S. 36. 36. 36. 3 12 3 2 2 - - 0 S. 36. 36. 36. 36. 36. 36. 36. 36. 36. 36. 36. 36. 37.		89	53	•	r	~	25	13	.3	yo.	¥	J	33.	
Wear 50 40 - 1 4 15 20 10 7 3 0 Lange 4 4 - - - - 9 3 0 - - 0 Sect Damage 126 381 381 381 381 382 340 152 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 172 161 114 47 114 47 114 47 114 47 114 47 114 47 114 47 114 47 114 47 114 47 114 47 114 47 114 47		81	92	,	-	60	33	8	1.	3	.1	0	•	
12 11 - - - 5 3 0 - - 0 0 0 0 0 0 0		20	3	ı	,-4	4	15	20	01	•	m	0	ر،	
S. Samuelle 4, 4, 4, 4, 4, 4, 2, 2, 38 1 1 3 0 0 0 0 0 0		12	11	•	•		sn	~	0	•	•	o	M.	
Street Damage 442 277 2 11 35 57 172 151 114 47 1 ed 126 91 1 - 3 27 60 30 11 47 1 e 126 91 1 - 3 27 60 30 11 4 6 4 7 1 <th></th> <td>4</td> <td>4</td> <td>•</td> <td>•</td> <td>•</td> <td></td> <td>e</td> <td>,</td> <td>•</td> <td>•</td> <td>ပ</td> <td>၁</td> <td></td>		4	4	•	•	•		e	,	•	•	ပ	၁	
SES 126 91 1 - 3 27 60 30 11 19 19 19 19 19 19 1	XTERMAL CAUSES	585	381	3	टा	3.8	9.8	04.7	367	\$2:	1 /9	741		
ed 126 91 1 - 3 27 60 30 11 19 1		442	277	7	11	35	57	172	191	11.4	1.	, 4	•	
se and Shipping Damage 15 11 - - - - - - - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - 0 - - <th>3. Overstressed</th> <td>126</td> <td>16</td> <td>7</td> <td>٠</td> <td>en</td> <td>27</td> <td>9</td> <td>30</td> <td>::</td> <td>61</td> <td>٠.</td> <td>,</td> <td></td>	3. Overstressed	126	16	7	٠	en	27	9	30	::	61	٠.	,	
se and Shipping Damage 15 11 - 1 - 4 6 4 3 1 0 SES 25 21 - - - - - 0 - - 0 SES 25 21 - - - - 0 - - 0 a 2 1 - - 1 1 1 1 1 1 0 a 219 390 8 16 24 100 242 106 51 55 2		2	7		•	٠	١	7	0	•	,	o	ø	
SES 25 21 - - - - - - 0 - - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 <th></th> <td>15</td> <td>11</td> <td>•</td> <td></td> <td>•</td> <td>4</td> <td>9</td> <td>4</td> <td>c</td> <td>.4</td> <td>0</td> <td>3</td> <td></td>		15	11	•		•	4	9	4	c	.4	0	3	
SES 23 21 - - 1 7 13 4 2 2 2 0 e 2 1 - - 1 1 1 1 2 0 23 20 - - 1 7 12 3 1 2 0 519 390 8 16 24 100 242 106 51 55 2		0	0		•	•	•	•	0	1	•	o	0	
23 20 - 1 7 12 3 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NO FAILURE CAUSES	25	17	=	=	1	-	13	77	2	2	O	0	
23 20 - 1 7 12 3 1 2 0 \$19 390 8 16 24 100 242 106 51 55 2		7	1	•	•	•	•	-4	-4	••	'	9	0	
519 390 8 16 24 100 242 106 51 55 2		23	20	•		1	7	12	3		2	0	S	
	UNICHOFIN CAUSES	615	390	••	91	77	일	242	106	52	5.5	ral	;;	

TABLE XXIV. SUPPARY OF REASONS FOR REMOVAL VERSUS REASONS FOR SCRAPPAGE OF UH-1C/AH-1G BLADES SCRAPPED AT BHC

Blades from Aircraft Model(s): UH-LC/A"-1G										Part No	•:	54.0-01001-5	3.
							REA	REASON FOR	SCRAPPAGE	351			
							\				3.4	3,6	
					\	\ ⁶ 9	* 477.	1 S. Journal	121.10	10			
REASON FOR REHOVAL		/	1.00	130	13.830	13.5		13	P. C.	13	V .	1	
	_		130	18	19.79.	Alog	40	10.24	Service .			1	E E
				*	; \	ζ,	\	*	, , ,		14.	1	/
ALL CAUSES	I X	102	e e	湘	91	ત્રા	ત્યા	최	:41	-11	-31	7 311	
1. PART CAUSES	53	23	71	٥١	;-1	7.1	3	9.	n	"	٥	~•	
A. Excessive Vibration	23	91	٠	~		10	.\$	ď	**	۳)	٠٠	= ,	
B. Deterioration	15	•	•	~			•	ž)	,	r 4		′ 4	
C. Bonding Failure	11	S		~	•	3	•	3	**	/4		()	
D. Excessive Mear	0	0	•	•		•	•	?	•	•	()	Ü	
E. Corrosion	4	۲,	7	•	C4	'	'		•		. •	J	
F. Other	0	0	•	•	•	,	•	0	١	•	٠,	c,	
II. EXTERNAL CAUSES	188	39	2	2	.4	61	' 1	:39	120	2)	O	رن	
A. Foreign Object Damage	170	32	•	ď		1:	v	5.4	115	1.		,	
B. Overstressed	17	^	7	rı	•	7		.31	.1	VI	• 1	•	
C. Heat Damage	0	0	,	•	•	•	•	Ω	,	•	ر)		
D. Maintenance & Shipping Damage	~1	0	,	•	•	•	,	. •		,	(,)	()	
E. Other	0	O	•	•	•	;	•	IJ	•	,	0	(,	
III. NO FAILURE CAUSES	12	7	'1	-1	1	4	71	- 1	1	÷.	::	m	
A. Time Change	1.8	7	•	-4	•	•	•	~1	. •	••	::	۳,	
B. Other	3	3	•	-	•	2	1	O	•	,	(0	
IV. UNKNOWN CAUSES	72	S	-	_2	7	21	اء	37	នា	L.J.	4	7:4	

TABLE XXV. THE COST OF BLADES TO REPLACE THOSE REMOVED

Type of Blades	204-011-250 (UH-1D/H)	204-011-250-5 (UH-1D/H)	540-01] (UH-1C,	540-011-001-5 (UH-1C/AH-1G)
	Basic	Adjus ted	Basic	Adjusted
Blades repaired by the user at the point of removal		\$ 47.12		\$ 48.79
Blades repaired in CONUS returned from S.E. Asia by:	\$ 925.00	34	\$ 787.00	
- Air Transport - Surface Transport		\$1424.09 \$1291.31		\$1308.69 \$1169.56
New Blades	\$2918.19	\$2944.25	\$3151.71	\$3177.75

The cost of a blade repaired at a repair facility is less than half of the cost of a new blade even when the repaired blade cost includes the apportioned shipping cost of the blades that were scrapped in CONUS.

The cost of a blade repaired at the point of removal is inexpensive compared to the facility repair, but the effectiveness of the field repair was not evaluated. (This would be difficult to determine.)

2. Aircraft Main Rotor Blade Support Costs

Table XXVI lists the aircraft blade support costs considering the different methods of transporting the blades, a 5000-hour aircraft life cycle and different blade replacement procedures. There is very little difference in support cost (18 to 20 cents per flight hour) between the methods of transportation used to ship blades for repair and to send new and repaired blades back to the user. (However, this would amount to \$180,000 to \$200,000 for a fleet flying a million flight hours under continued combat conditions.

If the CONUS repair procedure was stopped it would increase the support cost 89 cents per flight hour for the UH-1D/H and 56 cents per flight hour for the UH-1C/AH-1G.

With a low MTR relative to the AOT such as exists in a combat environment, a blade repair program is cost effective even when the scrap rate is high.

If the number of blades scrapped could be reduced or if the blades that are scrapped were scrapped at the point of removal, then the adjusted cost of the repaired blades could approach the basic costs shown on Table XXV.

TABLE XXVI. SOUTHEAST ASIA AIRCRAFT MAIN ROTOR BLADE SUPPORT COSTS

	Support Dramias	Dollars Per	Dollars Per Flight Hour*
		UH-1D/UH-1H	UH-1C/AH-1G
1.	Predicted cost based on the present repair/ replacement procedure - Air Transport both ways	\$10.02	18.418
6	Predicted cost based on the present repair/ replacement procedure - Surface Transport to CONUS and Air Transport to S.E. Asia	9.95	14.76
ะ	Predicted cost based on the present repair/ replacement procedure - Surface Transport both ways	9.84	14.61
÷	Ideal cost - Blades removed at AOT and Surface Transport of new blades to S.E. Asia	1.21	4.62
s.	No blade repair - new blades transported by Surface Transport	12.14	18.00
9	Blade repair at Organizational level only -	10.73	15.32

* For a 5000-hour aircraft life

V. CONCLUSIONS

A. MTR AND MIBR ANALYSES

The MTR analysis shows that for both UH-1D/H and UH-1C/AH-1G blades, the Vietnam combat and maintenance environment results in premature removals long before the allowable operating time is reached. On the average, the MTR is about 18 percent of the scheduled retirement life for the UH-1D/H blades and just over 30 percent for the UH-1C/AH-1G blades. A significantly longer life before removal is obtained when the aircraft is in a noncombat environment. Here a much larger percentage reach scheduled retirement and even more would if the aircraft did not have to contend with the training environment.

The blade MTR is a more understandable value than is the MTBR for use in comparing the reason-for-removal subgroups. Of course, it is necessary to have enough values to make the mean meaningful. The problem with MTBR values is that when the major reason-for-removal classes are divided into subgroups, the MTBR values increase (because fewer removals are divided into the same time base) and are difficult to evaluate.

Even though the blades have been improved as a result of field experience, the percentage of "part cause" removals (26.0% for the UH-1D/H and 24.1% for the UH-1C/AH-1G blades) indicates that further blade research is justified. The fact that the "part cause" MTR's for CONUS blades is 92 percent greater for the UH-1D/H and 23 percent greater on the UH-1C/AH-1G than for Vietnam "part cause" removals indicates that inadequate care and maintenance of the blades as well as the difference in natural environment may be important factors in the earlier removals of the Vietnam blades. This suggests that the design life of future blades should be free of preventive maintenance requirements, and the blade should be more resistant to the presently destructive elements.

B. SCRAP ANALYSIS

The probability of scrapping a blade removed for part or external causes is high. However, there does not seem to be a blade removal cause that consistently has a very low or zero repair history. More than 10 percent of the blades removed for part or external causes are repaired at the point of removal and are reinstalled on the aircraft from which they were removed, or are installed on other aircraft in the area.

requirement for major repair. But to be cost effective, the blade support cost would have to be less than the present cost. The blade cost targets (including the apportionment of engineering, tooling and test costs) are shown in Table XXVII. The method used to compute the cost targets is presented in Appendix C.

TABLE XXVII. COST TARGETS FOR THROWAWAY BLADES*

UH-1D/H	UH-1C/AH-1G
\$9.84/flt. hr.	\$14.61/flt. hr.
408.8 hrs.	315.5 hrs.
11.8%	16.1%
2360.85	2814.92
2082.27	2351.91
	\$9.84/flt. hr. 408.8 hrs. 11.8% 2360.85

D. GENERAL

As is often the case, as a study is completed, a review of the analyses that were performed and the information that was obtained suggest areas that should be studied in more detail or over a broader scale. Such is the case with this study. After this analysis was completed, several characteristics were noted that showed the need for additional study.

The results are very sensitive to the combat activities that occurred during the data period. For example, the TET offensive in January-February 1968 had a serious impact on the number of blades removed and the ratio of external to part cause removals.

By the time a group of blades gets to a repair facility, the reasons for scrappage of those that are scrapped do not necessarily correspond with the reasons for removal. Somewhere in the use-removal-return process the internal elements of most of the blades scrapped acquire water contamination, which will cause or may already have caused bond deterioration and corrosion.

C. AIRCRAFT MAIN ROTOR BLADE SUPPORT COSTS

The support costs would decrease if more of the blade repairs were accomplished in the field and if more of the blades that are scrapped were repaired. For this reason there has been concern about the number of blades scrapped and the desire for a more reparable blade for the UH-1/ AH-1 series aircraft. To date, no in-depth study has been made to determine the reparability of the existing The present criteria for blade damage inspection and reparability have been based on conservative estimates as to the diminished fatigue life produced by the damage (and wear) observed and the resulting repair, and the estimated cost of repair. A study should be made to determine blade reparability that includes the testing of blades already damaged. A second study should be made to evaluate blade repair cost (including the cost of the parts replaced) versus the allowable fatigue life remaining. This study should produce a repair cost formula that considers the remaining fatigue life. For example. it could be cost effective to perform an expensive repair on a low-time blade while a higher time blade requiring the same repair would be scrapped. These studies would be well worth their cost considering the millions of dollars expended for new blades. For a new blade designed for high reparability, the question that is unanswered is what the basic cost of such a blade would be. It could be quite expensive since such a blade would have to have redundant load members, removable panels, etc.

An alternative approach would be a less expensive blade with little or no capability for field repair and no

- The analysis of scrappage and repair of the UH-1D/H main rotor blades should be extended to include the data from Julian dates 7300 through 8199 so that a year of blade removals is included. The UH-1C/AH-1G blade analyses should be similarly expanded.
- Even though the data are inadequate to determine the probability of scrappage and repair on the 1969 removals, the 9000-9099, 9100-9199, 9200-9299, and 9300-9365 periods of removal data should be examined to determine whether the ratio of external to part cause removals and the MTR's are significantly different. These periods, compared with the similar periods in 1968, had a much lower combat rate that could affect the results of the analysis by showing that the support costs are decreasing. If this is so then the cost targets for a more reparable blade or a throwaway blade would be lower and more difficult to achieve.

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APPENDIX A

DEFINITIONS

1. Reasons for Removal

When components are removed from an aircraft for repair or replacement the data records prepared include a code for the reason for removal. The reasons for removal are grouped into four major cause classes for analysis purposes. They are:

- Part Causes
- External Causes
- No Failure Causes
- Unknown Causes

2. Part Causes

All reasons for removal that are the result of blade deterioration, i.e., excessive wear, bond separation, corrosion or blade unbalance, are grouped into the part cause classification.

3. External Causes

All reasons for removal that are the result of external forces damaging the blade or are due to stressing the blade beyond its specified limits are grouped into the external cause classification.

4. No Failure Causes

Reasons for removal that are "time change" or that are "other than for replacement or repair" are grouped into the "no failure" cause classification.

5. Unknown Causes

Records where reasons for removal are unstated or reasons that are inconsistent with blade removal, e.g., fuse blown, poor focus, etc., are grouped into the unknown cause classification.

6. Allowable Operating Time (AOT)

This is the number of flight hours that the blade is permitted to be used and still have an adequate fatigue life safety margin.

7. Mean-Time-To-Removal (MTR)

This value is the sum of the flight hours at removal for all blades divided by the number of blades removed. The MTR value will always be less than or equal to the AOT.

$$\sum_{i=1}^{i=n} t_i$$

$$MTR = \frac{i=1}{n}$$
(1)

where

t_i = The total flight hours on the ith blade at removal

n = The number of blades removed

8. Mean-Time-Between-Removals (MTBR)

The MTBR for main rotor blades is twice the sum of the flight hours of the group of aircraft from which the blades were removed divided by the number of blades removed during those flight hours.

$$\begin{array}{ccc}
j=m \\
2 & \sum t_{j} \\
MTBR & = \frac{j=1}{n}
\end{array}$$
(2)

where

t = The total flight hours of the jth aircraft

m = The number of aircraft in the group

n = The number of blades removed

9. Improved Blades

Improved blades are blades with cobalt leading edge abrasion strips, nonperforated honeycomb, improved bonding, sealed surfaces, etc. These are all UH-1C/AH-1G blades and all UH-1D/H blades with serial numbers A2-2400 and subsequent.

APPENDIX B

REASONS FOR REMOVAL AND SCRAPPAGE

TABLE B-I. MAIN ROTOR BLADE REMOVAL REASONS

			
	Reason For Removal	TAERS	RRAD OSM634
ALL CAU	ISES		***************************************
I.	PART CAUSES		
	A. Excessive Vibration Beyond specified tolerance Can't balance Erratic Excessive vibration Fluctuates, unstable Improper adjustment Improper alignment Improper contour Improper tracking Improper weight Mismatched Out of adjustment Out of position Unable to adjust limits	X X X X X X X X X	X X X
	Unstable B. Deterioration Brittle Burst Gracked Deteriorated Flaking Loose rivets	X X X X X	X X
	Loose trim tabs Noisy G. Bonding Failure Bond separation Delaminated Internal failure Loose Poor bonding	X X X	x x x x

TABLE B-I (Cont'd)

	Reason For Removal	TAERS	RRAD OSM 634
τ.	PART CAUSES (Cont'd)		
	D. Excessive Wear Brush failure/worn excessively Erosion	x	x
i I	Internal failure Pitted Split	x	X X X
	Worn excessively E. Corrosion Corroded	X X	x
	Deposits Leaking Moisture saturation	X X X	X X
	Rust or corrosion F. Other		X
11.	Manufacturing defect EXTERNAL CAUSES		X
	A. Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Chipped Collapsed Cut Damaged part, chip, nick, etc. Dented Foreign object damage Grooved Holes punched Mutilated Nicked Punctured Scored Torn	X X X X X X X	X X X X X X X
	B. Overstressed Broken weights Crash damage Hard landing Hit tree Jammed Overspeed	x x	X X X X

TABLE B-I (Cont'd)

	Reason For Removal	TAERS	RRAD OSM 634
II.	EXTERNAL CAUSES		
	B. Overstressed (Cont'd) Overstressed Overtorque RPM out of limit	x	X X X
	Sudden stoppage Warped	X X	X X
	C. Heat Damage Blistered Burned	X X	x
	D. Maintenance and Shipping Damage Bad patch, rivet, mod, tab, etc. Damaged in shipment	х	x x x
	Improper handling Improperly installed	х	X
	E. Other Failure caused by other component failures	x	
III.	NO FAILURE CAUSES		
	A. Time Change Allowable operating time	x	x
	B. Other Inspect, evaluate, or repair Lost or missing No failure Scheduled maintenance Wrong part		X X X X
IV.	UNKNOWN CAUSES		
	ļ.		

TABLE B-II. REASONS FOR SCRAPPAGE OF MAIN ROTOR BLADES AT BHC AND RRAD

Reason for Scrappage

ALL CAUSES

1. PART CAUSES

- A. Imbalance
 Beyond specified tolerance
 Bushing out of alignment
 Can't balance
 Tip or edge heavy
 Weights loose
- B. Deterioration Cracked Rough Worn
- C. Bonding Failure
 Bonding failure
 Core separation
 Delaminated
 Separated
 Void
- D. Corrosion Corroded
- E. Water Contamination Water in blade

II. EXTERNAL CAUSES

- A. Foreign Object Damage
 Bullet holes
 Creased
 Cut
 Damaged
 Dent
 Foreign object damage
 Holes
 Scored
 Torn
- B. Overstressed
 Bent
 Bowed
 Broken
 Buckled
 Crash damaged

TABLE B-II (Cont'd)

Reason for Scrappage

II. EXTERNAL CAUSES

B. Overstressed (Cont'd)
Crushed core
Distorted
Mutilated
Warped

III. NO FAILURE CAUSES

A. Time Change Allowable operating time

IV. OTHER CAUSES

A. Unknown

APPENDIX C

METHOD TO DETERMINE COST TARGETS FOR THROWAWAY BLADES

1. Analysis Method

To determine the cost target for throwaway blades in dollars per blade, values for the following functions should be established.

- The maximum desired aircraft main rotor blade support cost in dollars per flight hour
- The blade mean-time-to-removal for part and external causes at the location where the majority of the aircraft are stationed
- The percent of the blades removed for part and external causes that can be repaired at the point of removal
- The life cycle of the aircraft
- The number of blades per aircraft
- The cost of transporting the blades from the factory to the aircraft
- The average cost of removing and replacing a blade
- The average cost of repairing a blade at the point of removal

equation to compute the blade cost target was developed m equations (3), (5) and (6) in Section III of this report.

$$C_{T} = \frac{1}{g} \left[\frac{100 C_{b_{s}} L \widehat{MTR}}{n (L - \widehat{MTR})} - g \left(eC_{s_{a}} + fC_{s_{s}} \right) \right]$$

$$- 100C_{m} \left(T_{r_{1}} + T_{i} \right) + jC_{m} T_{r_{2}}$$
(1)

where

- C_T = The blade cost target, the cost of the new blade at the factory in dollars per blade
- C_b = Blade support cost in dollars per flight hour
 - L = Aircraft life cycle in flight hours
- MTR = The mean-time-to-removal for repair or replacement in blade hours
 - n = The number of blades in the rotor
- C_s = The dollar cost of shipping a blade to CONUS using air transportation
- C_s = The dollar cost of shipping a blade to CONUS using surface transportation
 - e = The fraction of the blades shipped from CONUS that are transported by air
 - f = The fraction of the blades shipped from CONUS by surface transportation
 - C_m = The manhour cost of organizational maintenance personnel
- T_r = The time in manhours to remove a blade assembly
- T_r = The time in manhours to repair a blade at the removal area
 - T_i = The time in manhours to install the blade assembly
 - g = The percentage of removed blades replaced by new blades
 - j = The percentage of the blades removed that are repaired by the using organization

For equation (1):

$$e + f = 1 \tag{2}$$

$$g + j = 100$$
 (3)

2. Examples

Two throwaway blade cost targets for the UH-ID/H and the UH-IC/AH-IG aircraft are computed to show how this method is used. The first target is based on a support program where limited blade repair is accomplished at the point of removal. The second is based on no repair. Table C-I presents the input values used for the computatations.

TABLE C-I. FUNCTION VALUES FOR THE EXAMPLE COMPUTATIONS

	Example			
Functions	L	2	3	4
Aircraft	UH-1D/H	UH-1D/H	UH-1C/ AH-1G	UH-1C/ AH-1G
C _{bs} - /flt hr	\$9.84	\$9.84	\$14.61	\$14.61
L - flt hrs	5000	5000	5000	5000
MTR - hrs	408.8	408.8	315.5	315.5
n	2	2	2	2
C _s	\$114	\$114	\$114	\$114
C _s	\$82	\$82	\$82	\$82
e	0	0	o	0
f	1	1	1	1
C _m	\$3.50	\$3.50	\$3.50	\$3.50
T _{r1} - hrs	3.73	3.73	3.72	3.72
T _{r2} - hrs	6.00	6.00	6.50	6.50
Ti - hrs	3.73	3.73	3.72	3.72
g	88.2%	100.0%	83.9%	100.0%
j	11.8%	0.0%	16.1%	0.0%

Table C-II presents the results of the computations.

TABLE C-II. RESULTS OF THE EXAMPLE COMPUTATIONS

	Mod el	
	UH-1D/H	UH-1C/AH-1G
Cost target of a blade capable of limited repairs at the point of removal (ground transportation, examples 1 and 3)	\$2360.85	\$2814.92
Cost target of a blade that is completely nonreparable (ground transportation, examples 2 and 4)	\$2082.27	\$2351.91

APPENDIX D

DETAILS OF REASON FOR REMOVAL/MTR/MTBR ANALYSIS OF TAERS DA2410 COMPONENT REMOVAL, AND REPAIR/OVERHAUL (AND INSTALLATION) RECORD DATA

TABLE D-I. REASON FOR REMOVAL/MIR ANALYSIS OF TAERS DA2410 D/H Main Rotor BLADE REMOVAL DATA

	Reason For Removal	Record	s With Time	Percent of All
		Number	MTR (Hours)	Causes
ALL CAUSES		8,222	453.5	100.00
I. PAR	T CAUSES	2,141	546.7	26.04
Α.	Excessive Vibration Beyond specified tolerance Excessive vibration Fluctuates, unstable Improper adjustment Improper alignment Improper tracking Improper weight Mismatched Out of adjustment Out of position Unable to adjust limits Unbalanced	521 27 173 6 4 1 34 5 34 21 1 119 73	355.1 443.7 298.1 432.8 895.5 499.0 277.9 241.6 366.0 498.9 178.0 401.4 367.4	6.34 0.33 2.10 0.07 0.05 0.01 0.41 0.06 0.41 0.26 0.01 1.45 0.89
В.	Unstable Deterioration Brittle Burst Cracked Deteriorated Flaking	23 698 8 7 608 69 6	278.3 597.3 428.8 994.0 585.6 671.3 689.5	0.28 8.49 0.10 0.09 7.39 0.84 0.07
c.	Bonding Failure Delaminated Internal failure Loose Poor bending	477 128 37 17 295	580.8 582.3 530.5 524.1 589.6	5.80 1.56 0.45 0.21 3.59
D.	Excessive Wear Brush failure/worn excessively Pitted Worn excessively	316 13 26 277	657.4 299.7 563.4 682.9	3.84 0.16 0.32 3.37
ε.	Corrosion Corroded Deposits Leaking Moisture saturation	129 76 7 28 18	648.9 749.0 339.0 486.2 599.1	1.57 0.92 0.09 0.34 0.22

TABLE D-I (Cont'd)

Number Number Causes All Causes		Reason For Removal		s With Time	Percent
A. Foreign Object Damage Battle damage (combat damage) Bent Broken Broken Buckled Chipped Collapsed Collap			Number		of All Causes
	III.	A. Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Chipped Collapsed Cut Dented Foreign object damage Grooved Nicked Punctured Scored Torn B. Overstressed Crash damage Overspeed Overspeed Overstressed Sudden stoppage Warped C. Heat Damage Blistered Burned Heat damage D. Maintenance and Shipping Damage Improperly installed E. Other Failure caused by other component failures NC FAILURE CAUSES A. Time Change Allowable operating time	4,425 752 74 74 37 23 184 1,198 754 10 49 883 95 742 162 234 118 196 32 15 9 5 1 1 1 5 5 87 87 87	398.8 398.5 386.8 409.8 426.3 472.6 433.8 68.6 346.5 437.6 416.5 328.7 406.7 357.8 652.0 366.8 400.4 485.1 392.6 297.8 412.5 330.5 349.7 394.4 238.4 504.0 106.0 106.0 583.6 583.6 1,658.8 1,658.8	53.82 9.15 0.90 0.90 0.45 0.28 0.04 2.24 14.57 9.17 0.12 0.60 10.74 0.11 4.56 9.02 1.97 2.85 1.44 2.38 0.39 0.18 0.11 0.06 0.01 0.01 0.01 0.06 1.06 1.06 1.06

TABLE D-II. REASON FOR REMOVAL/MTR ANALYSIS OF TAERS DA2410 C/G MAIN ROTOR BLADE REMOVAL DATA

	Reason For Removal		s With Time	Percent of
			MTR (Hours)	All Causes
ALL CAUSES		2.204	337.7	100.00
I. PAF	RT CAUSES	<u>532</u>	341.8	24.14
۸.	Excessive Vibration Beyond specified tolerance Erratic Excessive vibration Fluctuates, unstable Improper alignment Improper contour Improper tracking Improper weight Mismatched Out of adjustment	175 6 2 76 3 2 1 7	258.5 400.3 51.0 162.6 390.6 487.5 270.0 232.0 510.0 376.1 403.6	7.94 0.27 0.09 3.45 0.14 0.09 0.05 0.32 0.75 0.41
В.	Unable to adjust limits Unbalanced Unstable Deterioration Brittle	36 17 7 <u>148</u>	280.5 391.3 347.4 393.7 163.6	1.63 0.77 0.32 6.72 0.14
	Cracked Deteriorated Flaking	139 5 1	401.0 341.8 330.0	6.31 0.23 0.05
c.	Delaminated Internal failure Loose Poor bonding	118 23 15 12 68	341.6 288.4 710.9 135.8 314.4	5.35 1.04 0.68 0.54 3.09
D.	Excessive Wear Brush failure/worn excessively Pitted Worn excessively	60 3 1 56	412.4 386.6 66.0 419.9	2.72 0.14 0.05 2.54
Ε.	Corrosion Corroded Deposits Leaking Moisture saturation	31 22 4 3 2	427.5 414.0 368.2 618.6 406.5	1.41 1.00 0.18 0.14 0.09

TABLE D-II. (Cont'd)

	Reason For Removal		s With Time	Percent of
		Number	MTR (Hours)	All Causes
II.	EXTERNAL CAUSES	1,431	283.6	64.93
II.	EXTERNAL CAUSES A. Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Chipped Cut Dented Foreign object damage Grooved Nicked Punctured Scored Torn B. Overstressed Crash damage Overspeed Overstressed Sudden stoppage Warped	1,431 1,221 345 17 11 6 9 36 151 237 3 18 357 1 30 202 48 60 28 54 12		64.93 55.40 15.65 0.77 0.50 0.27 0.41 1.63 6.85 10.75 0.14 0.82 16.20 0.05 1.36 9.17 2.18 2.72 1.27 2.45 0.54
	C. Heat Damage Blistered Burned Heat damage D. Maintenance and Shipping Damage Improperly installed	-6 -3 1 2 -2 -2	201.0 357.3 84.0 25.0 488.5 488.5	0.27 0.14 0.05 0.09 0.09
III.	NO FAILURE CAUSES A. Time Change Allowable operating time	105 105 105	985.7 985.7 985.7	-4.76 -4.76 -4.76
IV.	UNKNOWN CAUSES	<u>136</u>	<u>388.7</u>	<u>6.17</u>

TABLE D-III. REASON FOR REMOVAL/MTR ANALYSIS OF TAERS DA2410 VIETNAM D/H MAIN ROTOR BLADE REMOVAL DATA

	Reason For Removal	Record Part	s With Time	Percent of All
		Number	MTR (Hours)	Causes
ALL CAU	SES	4,609	408.8	100.00
1.	PART CAUSES	1,069	519.5	23.19
	A. Excessive Vibration Beyond specified tolerance Excessive vibration Fluctuates, unstable Improper adjustment Improper tracking Improper weight Mismatched Out of adjustment Out of position	187 17 41 4 1 17 3 23 9	396.5 459.5 469.9 403.7 776.0 257.7 206.0 333.9 416.1 178.0	4.06 0.26 0.89 0.09 0.02 0.37 0.07 0.50 0.20 0.02
	Unable to adjust limits Unbalanced Unstable	43 28 5	486.5 284.4 297.6	0.93 0.61 0.11
	B. Deterioration Brittle Burst Cracked Deteriorated Flaking	375 5 2 316 48 4	538.8 515.4 806.5 516.3 675.3 576.2	8.14 0.11 0.04 6.86 1.04 0.09
	C. Bonding Failure Delaminated Internal failure Loose Poor bonding	238 57 15 5 161	515.5 512.8 353.3 399.2 535.1	5.16 1.24 0.33 0.11 3.49
	D. Excessive Wear Brush failure/worn excessively Pitted Worn excessively	177 12 19 146	594.2 293.1 551.1 624.5	3.84 0.26 0.41 3.17
	E. Corrosion Corroded Deposits Leaking Moisture saturation	92 58 5 19 10	557.5 668.8 315.6 412.3 308.2	2.00 1.26 0.11 0.41 0.22

TABLE D-III (Cont'd)

Reason For Removal			Percent
	Number	MTR (Hours)	of All Causes
EXTERNAL CAUSES	3,092	369.4	67.09
EXTERNAL CAUSES A. Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Chipped Collapsed Cut Dented Foreign object damage Grooved Nicked Punctured Scored Torn B. Overstressed Crash damage Overspeed Overstressed Sudden stoppage Warped C. Heat Damage Blistered Burned Heat damage D. Other Failure caused by other component failures NO FAILURE CAUSES A. Time Change Allowable operating time	3,092 2,616 512 41 46 13 15 2 136 725 373 7 22 493 7 224 464 86 143 75 143 17 8 5 2 1 4 4 4 4 4 4 4 4 4 4 4 4 4		67.09 56.76 11.11 0.89 1.00 0.28 0.33 0.04 2.95 15.73 8.09 0.15 0.48 10.70 0.15 4.86 10.07 1.87 3.10 1.63 3.10 0.37 0.17 0.11 0.04 0.02 0.09 0.09 0.09
	A. Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Chipped Collapsed Cut Dented Foreign object damage Grooved Nicked Punctured Scored Torn B. Overstressed Crash damage Overspeed Overstressed Sudden stoppage Warped C. Heat Damage Blistered Burned Heat damage D. Other Failure caused by other component failures NO FAILURE CAUSES A. Time Change Allowable operating time	Reason For Removal Part	Number Number Hours

TABLE D-IV. REASON FOR REMOVAL/MTR ANALYSIS OF TAERS DA2410 VIETNAM C/G MAIN ROTOR BLADE REMOVAL DATA

Reason	For Removal	Record Part	s With Time	Percent of All
		Number	MTR (Hours)	Causes
ALL CAUSES		1,288	315.5	100.00
I. PART CAUSES		<u>302</u>	<u>371.1</u>	23.45
Beyond Excessi Fluctua Imprope Imprope Imprope Mismato Out of	adjustment to adjust limits	86 23 1 1 1 6 4 7 22 12	324.6 360.2 304.1 268.0 201.0 270.0 248.5 390.0 511.2 281.4 375.6	6.68 0.39 1.79 0.08 0.08 0.47 0.31 0.54 1.71 0.93
Uns tab	oration	86 1 81	263.2 410.9 51.0 415.8 401.5	0.31 6.68 0.08 6.29 0.31
Delamir	al failure	70 13 8 2 47	340.3 295.2 569.6 321.0 314.5	5.43 1.01 0.62 0.16 3.65
Brush i	ive Wear failure/worn excessively ccessively	39 1 38	418.3 662.0 411.8	3.03 0.08 2.95
E. Corrosi Corrode Deposit Leaking Moistur	.a ⊤ :•	21 16 2 2 1	412.7 406.5 445.5 446.0 380.0	1.63 1.24 0.16 0.16 0.08
II. EXTERNAL CA	WSES	886	271.7	68.79
A. Foreign Battle Bent Broken Buckled	<u> Object Damage</u> Jamage (combat damage)	756 242 11 7 4	279.7 262.2 260.5 336.5 155.2	58.70 18.79 0.85 0.54 0.31

TABLE D-IV (Cont'd)

	Reason For Removal		e With Time	Percent
		Number	MTR (Hours)	of All Causes
II.	EXTERNAL CAUSES			
	A. Foreign Object Damage (Cont'd) Chipped Cut Dented Foreign object damage Grooved Nicked Punctured Scored Torn	24 88 158 3 14 185 1	386.2 325.2 283.5 263.2 76.3 338.4 291.8 432.0 455.6	0.31 1.86 6.83 12.27 0.23 1.09 14.36 0.08 1.16
	B. Overstressed Crash damage Overspeed Overstressed Sudden stoppage Warped	125 34 38 18 27 8	223.8 248.0 242.1 154.5 212.3 227.8	9.70 2.64 2.95 1.40 2.10 0.62
	C. Heat Damage Blistered Heat damage	$\frac{3}{1}$	117.7 303.0 25.0	0.23 0.08 0.16
	D. Maintenance and Shipping Damage Improperly installed	$-\frac{2}{2}$	488.5 488.5	0.16
111.	NO FAILURE CAUSES A. Time Change Allowable operating time	30 30 30	934.1 934.1 934.1	2.33 2.33 2.33
IV.	UNKNOWN CAUSES	_70	<u>365.2</u>	5.42
	,			

TABLE D-V. REASON FOR REMOVAL/MTR ANALYSIS OF TAERS DA2410 CONUS D/H MAIN ROTOR BLADE REMOVAL DATA

	Reason For Removal	Record	is With Time	Percent
	Reason For Removal	Number	MTR (Hours)	Of All Causes
ALL CAUSE	S	333	993.4	100.00
I. <u>P</u>	ART CAUSES	148	994.5	44,44
^	Excessive Vibration Beyond specified tolerance	35	532.2 662.5	10.51
1	Excessive vibration Mismatched	12 1	226.3 161.0	3.60 0.30
	Out of adjustment Unable to adjust limits	2	610.5	0.60 2.40
	Unbalanced Unstable	8 2	970.3	2.40 0.60
В			1,140.5	16.82
	Burst Cracked	52	436.0 1.136.4	0.30 15.62
	Deteriorated	3	1,100.6	0.90
C	. Bonding Failure Delaminated	<u> 36</u>	1.000.3	10.81 1.80
	Internal failure	1.	1,732.0 858.5	0.30 1.20
	Poor bonding	25	920.3	7.51
D	. Excessive Wear Worn excessively	18	1,556.4	5.41 5.41
E	. <u>Corrosion</u> Deposits	-3	835.3 222.0	0.90
	Leaking	2	1,142.0	0.60
II. E	KTERNAL CAUSES . Foreign Object Damage	134 76	765.6 796.0	40.24 22. 8 2
^	Broken		1,591.0	0.30
	Buckled Chipped	1 3	196.0 673.7	0.30 0.90
	Dented Foreign object damage	51 4	838.4 487.8	15.32 1.20
	Nicked Punctured	4 3 4	672.3 559.8	0.90 1.20
	Torn	9	858.0	2.70
В	Overstressed Crash damage	_ <u>58</u> 26	725.7 940.4	17.41 7.81
1	Overspeed	10	533.0	3.00

TABLE D-V (Cont'd)

	Reason For Removal		la With Time	Percent Of All
		Number	MTR (Hours)	Causes
II.	EXTERNAL CAUSES B. Overstressed (Cont'd) Overstressed Sudden stoppage Warped	6 14 2	348.0 691.5 272.0	1.80 4.20 0.60
III.	NO FAILURE CAUSES A. Time Change Allowable operating time		2,396.9 2,396.9 2,396.9	8.41 8.41
IV.	UNKNOWN CAUSES	23	604.6	6.91
Ť				
1 1				

TABLE D-VI. REASON FOR REMOVAL/MTR ANALYSIS OF TAERS DA2410 CONUS C/G MAIN ROTOR BLADE REMOVAL DATA

	Reason For Removal	Record	e With Time	Percent
<u> </u>		Number	MTR (Hours)	of All Causes
ALL CAU	SES	53	475.7	100.00
ı.	PART CAUSES	18	455.3	33.96
	A. Excessive Vibration Excessive vibration Unable to adjust limits Unbalanced Unstable	8 2 2 1 3	509.1 359.0 668.5 639.0 459.6	15.09 3.77 3.77 1.89 5.66
	B. Deterioration Cracked	-5	544.8 544.8	9.43
i	C. Bonding Failure Delaminated Poor bonding	-2 1	97.0 16.0 178.0	3.77 1.89 1.89
	D. Excessive Wear Worn excessively	$\frac{2}{2}$	$\frac{371.0}{371.0}$	3.77 3.77
	E. <u>Corrosion</u> Corroded	+	462.0 462.0	1.89
II.	A. Foreign Object Damage Buckled Chipped Cut Dented Foreign object damage Torn B. Overstressed Overspeed	22 16 1 1 1 9 1 3 6 6	290.2 232.0 126.0 72.0 395.0 192.4 18.0 456.3 445.3	41.51 30.19 1.89 1.89 1.89 1.89 5.66 11.32 11.32
111.	NO FAILURE CAUSES	<u>10</u>	994.7	18.87
	A. Time Change Allowable operating time	10 10	994.7 994.7	18.87 18.87
IV.	UNKNOWN CAUSES	_3	229.3	5.66

TABLE D-VII. REASON FOR REMOVAL/MTR/MTBR ANALYSIS OF A SELECTED SAMPLE OF TABLES DA2410 VIETNAM D/H MAIN ROTOR BLADE REMOVAL DATA

	Reason For Removal	Record	e With Time	Levron.
·	Readon Por Removal	Number	M7R (Hours)	MTBR (Hours)
ALL CA	US ES	136	514.3	1,063
	RT CAUSES	_26	601.0	5,560
۸.	Excessive Vibration Unable to adjust limits	$\frac{2}{2}$	98.0 98.0	72,278 72,278
В.	Deterioration Cracked	-8	565.6 565.6	18,070 18,070
c.	Bonding Failure Delaminated Internal failure Poor bonding	15 6 3 6	667.6 269.0 856.7 471.7	9,637 24,093 48,185 24,093
D.	Excessive Wear Pitted	-1	891.0 891.0	144.556 144,556
E.	Corrosion	0	0.0	
P.	<u>Other</u>	_0	0.0	<u></u>
II. <u>ex</u>	Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Chipped Cut Dented Foreign object damage Punctured Torn Overstressed Overspeed Overstressed	109 102 21 1 1 28 17 22 7	494.8 484.8 598.9 495.0 235.0 218.0 600.0 216.3 433.2 697.4 370.6 362.1 641.1 467.0 418.1	1,326 1,417 6,884 144,556 144,556 144,556 144,556 48,185 5,163 8,503 6,571 20,651 20,651 36,139 144,556
c.	Sudden stoppage	2 _0	1,101.0	72,278
D.			0.0	•
E.		익 이	0.0	-

TABLE D-VII (Cont'd)

Reason For Removal	Record	with Time	MTER
	Number	MTR (Hours)	(Hours)
III. NO FAILURE CAUSES	0	0.0	
IV. UNKNOWN CAUSES	1	385.0	144,556
	<u>.</u> L		
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	i		
	1		

TABLE D VIII. REASON FOR REMOVAL/MTR/MTBR ANALYSIS OF A SELECTED SAMPLE OF TAERS DA2410 VIETNAM C/G MAIN ROTOR BLADE REMOVAL DATA

	Reuson For Removal	Record	s With Time	MTBR
		Number	MTR (Hours)	(Hours)
ALL	CAUSES	<u>250</u>	279.1	908
I.	PART CAUSES	63	348.3	3,602
	A. Excessive 4ibration Beyond specified tolerance Excessive vibration Fluctuates, unstable Improper tracking Out of adjustment Unable to adjust limits	20 1 6 1 1 1 8	266.0 682.0 266.0 268.0 405.0 49.0 249.1	11,346 226,920 37,820 226,920 226,920 226,920 28,365
	Unbalanced B. Deterioration Brittl: Gracked Deteriorated	2 19 17 1	424.0 382.7 51.0 417.9 121.0	113,460 11,943 226,920 13,348 226,920
	C. Bonding Failure Delaminated Internal failure Poor bonding	17 4 3 10	299.2 265.5 423.3 275.5	13,348 56,730 75,640 22,692
	D. Excessive Wear Brush failure/worn excessively Worn excessively	$\frac{3}{1}$	821.3 662.0 901.0	75,640 226,920 113,4
	E. Corrosion Corroded Leaking	-4 3 1	462.0 518.3 293.0	56,730 75,640 226,920
	F. Other	_0	0.0	
11.	EXTERNAL CAUSES	181	236.7	1,252
	A. Foreign Object Damage Battle damage (combat damage) Bent Broken Cut Dented Foreign object damage Punctured Torn	141 35 3 1 4 15 18 62 3	227.5 173.5 165.0 288.0 415.3 227.1 268.0 242.3 101.3	1,609 6,483 75,640 226,920 56,730 15,128 12,607 3,660 75,640
	B. Overstressed Crash damage	<u>38</u>	257.7 174.5	5,972 56,730

TABLE D-VIII (Cont'd)

	Reason For Removal		e With Time	MTBR
		Number	MTR (Hours)	(Hours)
III.	EXICANAL CAUSES B. Overstressed (Cont'd) Overspeed Overstressed Sudden stoppage Warped C. Heat Damage D. Maintenance and Shipping Damage Improperly installed E. Other NO FAILURE CAUSES A. Time Change Allowable operating time B. Other UNKNOWN CAUSES	18 13 2 0 2 2 0 4 4 0 2		12,607

TABLE D-IX. REASON FOR REMOVAL/MTR/MTBR
ANALYSIS OF A SELECTED SAMPLE
OF TAERS DA2410 CONUS D/H
MAIN ROTOR BLADE REMOVAL DATA

			•	
	Reason For Removal	Record	s With Time	MTBR
		Number	MTR (Hours)	(Hours)
ALL	CAUSES	16	1,484.1	720
I.	PART CAUSES	_6	853.8	1,919
	A. Excessive Vibration Unable to adjust limits Unstable	3 1 2	696.0 1,940.0 74.0	3,839 11,516 5,758
	B. <u>Deterioration</u> Cracked Deteriorated	$\frac{3}{2}$	1,011.7 638.0 1,759.0	3,839 5,758 11,516
	C. Bonding Failure D. Excessive Wear	0 0 0	0.0	
i	E. Corrosion	0	0.0	-
	P. Other	0	0.0	<u> </u>
11.	EXTERNAL CAUSES	<u>4</u>	951.5	2,879
	A. Foreign Object Damage Dented	4 4	951.5 951.5	2,879 2,879
1	B. Overstressed	_0	0.0	
.	C. Heat Damage	_0	0.0	-
İ	D. Maintenance and Shipping Damage	9999	0.0	
	E. Other	_0	0.0	
111.	NO FAILURE CAUSES	_6	2,469.3	1,919
	A. Time Change Allowable operating time	<u>6</u>	2,469.3 2,469.3	1,919 1,919
	B. Other	_0	0.0	
IV.	UNICHOWN CAUSES	0	0.0	

REASON FOR REMOVAL DISTRIBUTION COMPARISON OF THE TAERS DATA FILES AND THE DATA SAMPLES SELECTED FOR MTBR ANALYSIS TABLE D-X.

ļ																			
			CH-1 C	UH-1C/AH-1G		- VIETNAM			3	A - 22 C'-350	VIETU	3			5	B 31-85	1	1	
	Reason for Removal	VI	All Ships		Moni	Monitored Ships	sdiu	4	Ail Snips		Var i	Var itores	\$ 27.45				a).	;	5
		%o.	HTR	,,	No.	Ĕ		ķ	K; X	4,	.×.	Ę	ļi		Ϋ́			ij	
77.	ALL CAUSES	2.204 337.7	337.2	100.00	250	279.1	.co.vo	9,222	-53.5	30.30	3	5.4.3	CC 14	3			1		
1:	I. PART CAUSES	532	532 341.0	24.14	63	26.3	25.20	2,141	546.7	3.02	77	35		1	!	,	Ŀ		
	A. Excessive Vibration	175		7.34	20	266.0		\$2	355.1			3.85		1 %	:33	J:	1 -	:	7
	B. Deterioration	148	148 393.7	6.72	3	382.7	5.60	869	597.3		2,	3.5.5		%		•	~	•	•
	C. Bonding Failure	118	118 341.6	5.35	11	299.2	5.60	477	580.8	3.30	. 5	9.7.5		÷		,	•		,
	D. Excessive Wear	09	412.4	2.72	•	521.3	20	316	6.57.4	#. m	•	0.161	£	•	57:	•	,		j
	E. Corresion	3:	3: 427.5	1.41	3	462.0	1.60	5	0.46.	\$3. F	7		3.0	r,	-1	3	U	,	5
.11	EXTENDAL CAUSES	1,431 253.0 64.93	253.6		181	236.7	72.40	5,185	395.8	635	. 6.9	8 27 B	8	3		0.0	ľ		:
	A. Poreign Object Damage	1,222 285.4	285.4		191	227.5	\$6.440	4.425	398.5			3. 46.	3.5.	۴	;		•	,;	5
	B. Overstressed	202	202 273.1	9.17	38	257.7	15.20	7+2	*009	3.62	Ť	:: 2		#1 w 1			7	,	
	C. Heat Demage	9	6 201.0	0.27	0		o.0	13	347.7	C		•	5.5	4		000	٠	,	
	D. Maintenance and Shipping	7	2 468.5	9. °C	74	488.5	°.	••	100.0	3.6	J	•		ن	•	ů,	,	-	•,
	E. Other	0	•	8.3	0	•	9.8	\$	593.2	0.0	5	•	,	()	,	3			,
111.	III. NO FAILURE CAUSES	105 985.7	2.28	4.76	7	1.184.8	1.60	87	1,559.5	40.1	0		ල් ස			•		ÿ	
	A. Time Change	105	105 945.7	4.76	9	1.104.9	60	87	i.e50.5	š:-	37	·	30.0	7	7 44 6		_	•	,
17.	UNICHOUN CAUSES	136 388.7	300.7	6.17	2	123.5	0.60	305	428.4	30	1	3.5.5	0.00	7	2.4		4	,	

Improved Blades Only
 FY '65 AH-1G Aircraft Data Only
 FY '65 and '66 Aircraft Data Only

APPENDIX E

DETAILS OF REASON FOR REPAIR OR REPLACEMENT ANALYSIS OF UH-1/AH-1 MAINTAINABILITY AND RELIABILITY PROGRAM FIELD FAILURE/DISCREPANCY REPORT DATA

REASON FOR REPAIR OR REPLACEMENT/MIBR	ANALYSIS OF UH-1D/H M & R PROGRAM	MAIN ROTOR BLADE FAILURE REPORT DATA
TABLE E-I.		

Blade P/8 206-011-250-5		9pe ::	Time Base	FORT RUCKER, ALABAMA ade Time Base a 6324 Fluint dours	Lant de	٤			412 477	100 mm	100 P p	4. 7 H U		
Ressons for Repolr or Replacement	Muster H-T-B Repaired Repairs or or Replaced Replace	Mumber N.T.B Mumber Repairs Remova- or for Replaced Replace Papair	Number Removed for Repair or Repl.	M-I-B Removala for Repair or Repl.	Number of Replaned	K-I-B	Fee. n. Fee. n. Fee. scar	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		N	a			
1. 2481 CAUSES	44	न्यः चन्न	ं ०	: :	ç	; ;	0 0 0	3 ::	7 8	; ; ::		: :		1
A. Sacasaiva Vibration	э	:	61	:	o	:		- 10-1	33		800 117	٠	\$ 1. 3 1.	11:
B. Beterigration	ઝ	:	O)	:	CI	;	:	61	;	ЭI	;	(M	;	:
C. Pending Pailure Lend Separation at	o#	:	c)	:	OI.	:	:	214		21*	7.	:1"	1	Ŀ
Tip cap separated Trim tab unborded										7	200		306.**	- M
D. EMECSBIVE dear Senier chipped at trim tab	rd-r	#	calco .	::	c#o	::	3::E	e1	:	Ci	P	4		
II. EXTENDE CAUSES	-4	2912	c	;	0	:	2.00.1	-	= -	; j	::	:		-:
A. Parties Chier Dente Barte dange Dente from and bage Hit entenna Hit spent bras:	d	:	æ	;	~	:		ne a a a	17.200	and the	1000	710 mm	11000	3 1 ***;
Systemated	74	7577	ct	:	ca.		2000	:11	1	.21	法	.11	37.1	1
Overspeed (at auto-	N	23.62	۰	:	5	:	100.0		3	2	:	•		•
C. Maat Depare	ส	:	ci	;	01	:	:	31	;	~	:	cd	:	3
D. Maintenance and Phisping Denace	2	:	લ	:	વ	:	:	sı	;	(I	;	44	;	,

TABLE E-II. REASON FOR REPAIR OR REPLACEMENT/MTBR ANALYSIS OF "H-1C M & R PROGRAM MAIN ROTOR BLADE "LIJNE REPORT DATA

Blade P/H 540-011-001-005		Blade	FORT Blade Time Bar	RUCKER, ALABAMA se = 25,544 Flight Hours	ALABANA Sub Plight	Hours			Blade	Time Base	VIETNAM Blade Time Base x 29,676 Filght Mours	Tagar.	2 2	
Resons for Repair	Bumber	N-T-B	Number .	H-T-B	Number Per legal	M-T-M	_	Number	H-T-B	Number	H-T-B	. eps	4 H	Percent
or Peplacement			for	Į d		- 83			2	101	Į,		hep.a.e.	וש: בניפתו
	Peo P de	Per t	Mepair or Repl.	Repair or Repl.		ment s	Meplace-	re placed	Replace-	Repair or Repl.	depair		Bent s	
ALL CAUSES	7	11111	==	1,419	17	1,503	26.1	97	\$:	724	*	22.	30.9
1. PART CAUSES	듸	1,965	=	2,322	2	2.5%	23.1	^	2.968	^	2.964	-	335.2	0.0
A. Bressive Vibration Camor track	940	柔	040	2.63.5 2.63.5	040	2.53.5 SEE: 5	့ဂ	ele	\$1.7.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	ala	N.	- e l e	季	ွန
B. Paterioration	a	:	ø	ŀ	al	;	:	ol	:	ol	:	Θl	:	:
C. Post for Pallyrs Ford Separation at	N	14:73	MN	13.773	-4-	12:773	000 000 000 000 000 000 000 000 000 00	4	29.676	 - -	2.6.5 2.6.5	i valja	\$ \$ \$	ွော ဝင်
D. Willer erveled at UE	MN	12.772	010	::	olo	;;	69 69 9	ol	;	ol	;	ol	:	:
II. EXTERNA CAUSES	의	2,5%	1	3.549	۱-	3,649	30.0	3	72.	*	9.20	36	:	::
A. Porsign Object Denses Lattle dange Cute	~	2777	4	3.244	-4	23.25th	ુ જ	SIE -	26.086 6.78.	XIZ	20.05	ar.		
Dents Holes Scratches		33.	0 =	25.54	0-1	25.5	100.0	-4	29.676		29.676	-1	29.676	u
B. Overstrased Hit tree Hit washown object Overspeed (engine) Overspeed (autorotation)	eluna y	42.5°5	4	7555°	10 to	25.55	%0000 00000	ala	9 892	nIn	\$. 89 2 5 . 8 2 2	nh		ပည ဝါဝ
C. Heat Design	a	:	о	;	ol	:	;	01	;	ol	1	οl	:	:
D. Maintannes & Shipping	oł	:	ot	:	oı	;	:	01	3,710	©	3.710	•1	3.7.0	31
Red-patch Bent by sling Grack at repair Maintehance arrer									29.676 29.676 7.619 14.838	2 0	22.2	4N		0000

TABLE E-III. REASON FOR REPAIR OR REPLACEMENT/HTBR ANALYSIS OF AH-1G M & R PROGRAM MAIN ROTOR BLADE PAILURE REPORT DATA

Blade P/W 540-011-001-005		Blade	Time Bes	ě.	Flight	Nours			Blade	Tim Base		VIETHOR	E ur	
Masons for Aspair or Asplacement	Parities	N-T-8 Repairs Of Replace-	for the pie.	M-T-B Memovals for Mapair or Mapl.	Rumber Rep Laced	N-T-B Replace-	Percent Repaired (Vithout Seplace-	Mumber Mepaired or or	N-T-B Repairs or Replace- ment	Mumber Reflected for Renair or Repl.	N-T-B Removals for Repair or Repl.	Meber Replaced	N-7-8 Replace- sents	Percent Repaired (Vithout Replace-
ALL CASES	#	1.507	717	1,407	21	1,630	9.5	:115	982	100	:,010	:	1:00	22.6
PART & SKIESPAL CAUSES	3	3	2	307	21	2,382	3	3		8	1.014	21	3	22.6
1. PART CAUSES	4	3.879	4	3.870	٠	5,162	25.0	n	3.273	22	3.78	*	3.902	1:91
A. Sessairs Vibration Cannot belance Lateral vibration	a	:	ol		оі	:	:	a Hin	101.25	alun	101.00 101.00 101.00	nun	101.5% 50.720	35.0
B. Briggiannian	+	***	+	樂湖	+	36.98 19.98	of:	*	***	r.p.	业	r#r	继	90
C. Beatlac Pailurs Send separation at	*	Ŧ	**	Ŧ	-tn	#	Ľ	¥	36.36	#	**************************************	æ	18. S.	\$.5 2
Bond your Identification plats slost og	٠.	15,462		5.2	•	15,482	000	91	10,146	•	16.909	•	16.90	0.0
O. Personales Mag. of Lot	***	#	n 4m	1	010	::	9.00	~	162.05	~	ास- १	~	1071	g
Leading edge erosion								*	20.291	•	20.781	•	29.22 12.02	0.0
II. STEEPS CAUSES	4	4,423	시	6,423	-1	6,623	0.0	4	1.208	r!	1,390	3	1.610	25.0
A. Paries Oblect Bears		15.462	~	15.482	~1	15,482	잉	≈ C -	F	312	\$ 1.536	212	: ***** *******	Ŧ
Dant Persign object dange Mit T/R driveshaft cor-		35.0		30.964		24 24 25	000	. ~	8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	, m.m.m	8.000.00	B	****	90000
P. Oranizates	al	7,761	41	147.7	*1	7.781	្ង	r	***	r	Ŧ,	×	北	90
The state of the base		174 828		171 828		171 R2R	000	~~•~~	25.72 26.53 26.72 27.73 27.73	N-4 N-N	8 5 5 8 5 8 8 8 5 8 5 8 8 8 5 8 5 8	n-•n-n	35235 235232	

TABLE E-III (Cont'd)

Blade P/W \$40-011-001-005		Blade	HUNTER Blade Time Bas	HUNTER ARMY AIR FIELD We Base + 30,964 Flight Hours	FIELD Flight	Hours			Blade	T.ze Base	Blade Time Base - 151.455 Flight Mours	e Fight	Hours	
Massons for Aspair or Asplacosm	Number M-1-8 Repaired Repairs or Replaced Replace-		Number Removed for Repair or Repl.	M-I-B Removals for Repair or Repl.	Number Replaned	M-I-B Roplace- Tenta	Percent Resarred (at thous Replace	Recorded Republication	Section 19-38	Name of the relation of the relationship of th	P. 7-B New Cr. Bracockis Re, seers for Repair or Rec.	V. R. CF. Re, . seers	# 7 - B	Ferrent Former France France France
(P. AWD) THENT CHEET (CHE. P.)														
C. Best Desert	a	:	ol	:	cl	:	:	-	:	ର	;	÷οΙ	٠	;
Design	4	30,964	~4	30,964	1	30,964	ુ	31	7.34.7	괴	7	21		3]
Gracing of patched hole	- -							41.0	25.364	31.0	15.36	***	25.25 26.25 26.25	330
Maintenance denage Trie tab tern by sling	-	36.08	-	30,964	-	30,964			17.456		101.456	•	101.456	
E. Other.	ø	:	01	:	cıl	:	;	rape	55. 1C1	ral	10:53	(plant	\$5.73	:K
Hit by ness ompartment cover								-1	101.456	**	101,456		101.	0.5
III. IN PAILING CANSES	4	7.761	-	7.743	4	7,741	٥. ٥	2	:	ပ	:	၀	;	:
A. Honoble operating time	414	李	212	恋	ala	 	် လိုင်	-						
IV. MEDIOME	7	15.482	7	15.482	"	15,482	0.0	۲	:	٥	:	ū	;	:

APPENDIX F

DETAILS OF REASON FOR REMOVAL/MIR ANALYSIS OF BELL HELICOPTER COMPANY AND RED RIVER ARMY DEPOT MAIN ROTOR BLADE REPAIR AND SCRAP DATA

TABLE F.I. REASON FOR REMOVAL MIR ANALYSIS OF D/H MAIN ROTOR BLADES REPAIRED OR SCRAPPED AT BHC AND SCRAPPED AT RRAD

	Reason For Removal	Record Part	s With Time	Percent of All
		Number	MTR (Hours)	Causes
ALL CAU	SES	2,820	428.3	100.00
1.	PART CAUSES	464	450.8	16.45
	A. Excessive Vibration	105	340.4	3.72
	Beyond specified tolerance Cannot balance	- - 5	481.2 339.2	0.18 2.27
	Erratic	1	95.0	0.03
	Excessive vibration	35	329.4	1.24
	B. Deterioration Cracked	102 83	449.7 447.5	$\frac{3.62}{2.94}$
1	Deteriorated	15	461.0	0.53
	Loose rivets Noisy	2 2	556.5 348.5	0.07 0.07
	C. Bonding Failure	155	457.2	5.50
	Bond separation	117	451.4	4.15
	Delaminated Loose	26 10	461.6 531.4	0.92 0.35
ľ	Poor bonding	2	366.0	0.07
	D. Excessive Wear	78	537.6	$\frac{2.77}{2.13}$
1	Erosion Internal failure	60 7	530.1 588.0	0.25
	Pitted	4	540.2	0.14
	Worn excessively	7	550.1	0.25
	E. Corrosion Deposits	<u>19</u>	709.0 359.0	$\frac{0.67}{0.11}$
	Leaking	1	530.0	0.03
	Rust or corrosion	15	790.9	0.53
	F. Other Manufacturing defect	-5	258.0 258.0	0.18
11.	EXTERNAL CAUSES	1,324	364.9	46.95
	A. Foreign Object Damage	908 218	372.5	32.20
	Battle damage (combat damage) Bent	7	430.6 373.9	7.73 0.25
	Broken Buckled	6	442.3	0.21 0.18
	Collapsed	5 1	284.4 6.0	0.18
	Damaged part, chip, nick, etc.	299	342.0	10.60
1	Dented	233	379.1	8.26

TABLE F-I (Cont'd)

			le With Time	Percent
	Reason For Removal	Mumber	MTR (Hours)	of All Causes
11.	EXTERNAL CAUSES			
	A. Foreign Object Damage (Cont'd) Foreign object damage Holes punched Mutilated	81 58 0	321.9 361.7	2.87 2.06 0.00
	B. Overstreused Crash damage Hard landing Hit tree Jammed Overstressed Overtorque RPM out of limit Sudden stoppage Warped	390 136 6 1 1 31 2 162 49	345.1 395.4 410.5 620.0 378.0 248.0 132.5 328.6 310.1 493.6	13.83 4.82 0.21 0.03 0.03 1.10 0.07 5.74 1.74 0.07
	C. Heat Damage Blistered Heat Camage	-4 1 3	494.0 765.0 403.7	0.14 0.03 0.11
	D. Maintenance and Shipping Damage Bad patch, rivet, tab, etc. Damaged in shipment Improper handling	22 18 0 4	378.5 383.6 355.5	0.78 0.64 0.00 0.14
	E. Other	0		0.00
m.	NO FAILURE CAUSES	40	805.7	1.42
	A. <u>Time Change</u> Allowable operating time		2,064.6 2,064.6	0.28
	B. Other Inspect, evaluate, or repair Lost or missing No failure Scheduled maintenance	32 4 8 16 4	491.0 435.8 350.2 558.4 557.8	1.13 0.14 0.28 0.57 0.14
IV.	UNKNOWN CAUSES	<u>992</u>	487.3	35,18

TABLE F-II. REASON FOR REMOVAL/MTR ANALYSIS OF C/G MAIN ROTOR BLADES REPAIRED OR SCRAPPED AT BHC AND SCRAPPED AT RRAD

		Discoura Home Removal		s With Time	Percent
		Reason For Removal	Number	HIR (Hours)	of All Causes
ALL CAU	SES		925	341.5	100.0
1.	PAR A.	Beyond specified tolerance Can't balance Erratic Excessive vibration Mismatched Deterioration Cracked Deteriorated Loose rivets Loose trimtabs	135 74 2 45 2 24 1 28 21 4 21 16 2	349.7 323.4 715.5 328.2 345.0 277.9 374.0 321.2 396.2 70.0 276.0 64.3 351.9 377.0 20.5 439.3	14.6 8.0 0.2 4.9 0.2 2.6 0.1 3.0 2.3 0.2 0.1 0.4 2.3 1.7 0.2 0.3
	D.	Excessive Wear Erosion Internal failure Worn excessively Corrosion	6 1 2 6	647.2 746.0 504.0 570.5	0.7 0.3 0.1 0.2 0.7
į	€.	Rust or corrosion	<u> </u>	502.0	7.7
	F.	Other	<u> </u>	286 6	0.0
II.	A.	Foreign Object Demage Battle damage (combat damage) Bent Cut Demaged part, chip, nick, etc. Dented Foreign object damage Holes punched Mutilated Overstressed Broken Weights	512 424 236 3 1 77 33 26 47 1	286.6 292.3 294.1 319.3 395.0 307.4 270.9 261.6 291.7 36.0 268.5 599.0	55.4 45.8 25.5 0.3 0.1 8.3 3.6 2.8 5.1 0.1 9.0

TABLE F-II (Cont'd)

Reason For Removal		le With Time	Percent of All
	Number	MTR (Hours)	Causes
B. Overstressed (Cont'd) Crash damage Hard landing Hit tree Overstressed RPM out of limit Sudden stoppage C. Heat Damage Damaged in shipment Improper handling E. Other III. NO FAILURE CAUSES A. Time Change Allowable operating time B. Other No failure Scheduled maintenance IV. UNKNOWN CAUSES	13 5 3 8 33 20 0 5 0 5 0 57 41 41 16 15 1	265.3 188.2 301.0 324.3 245.8 284.5	1.4 0.5 0.3 0.9 3.6 2.2 0.0 0.5 0.0 6.2 4.4 1.7 1.6 0.1 23.9

TABLE F-III. REASON FOR REMOVAL MIR ANALYSIS
OF D. H MAIN ROTOR BLADES REPAIRED
OR SCRAPPED AT BHC

	Reason For Removal ALL CAUSES		Record Part	a With Time	Percent of All
			Number	(Hours)	Chunes
ALL CAL	SES		2,305	408.7	100.00
1	PAR	T CAUSES	459	445.1	19.91
i	A.	Excessive Vibration	105	340.4	4.56
		Beyond specified tolerance Cannot balance	5 64	481.2 339.2	7,22 2,78
		Erratic	1	95.0	0.04
1		Excessive vibration	35	329.4	1.52
	B.	Deterioration	102	449.7	4.43
		Cracked Deteriorated		447.5 461.0	3.60 0.65
		Loose rivets	2	556.5	0.09
		Noisy	2	348.5	0.09
	C.	Bonding Failure	153	<u>453.1</u>	6.64
}		Bond deparation Delaminated	TT5 26	445.9 461.6	4.99 1.13
		Loose	10	531.4	0.43
		Poor bonding	2	366.0	0.09
	D.	Excessive Wear	78	537.6	3.38
		Erosion Internal failure	60 7	530.1 588.0	2.60 0.30
1		Pitted	4	540.2	0.17
ſ		Worn excessively	7	550.1	0.30
	£.	Corrosion	<u> 16</u>	634.4	0.69
		Deposits Leaking	- 3 1	359.0 530.0	0.13
		Rust or corrosion	12	712.0	0.52
	F.	Other	5	258.0	0.22
	•	Hanufacturing defect	- <u>5</u>	258.0	0.22
II.	EXT	TERNAL CAUSES	979	343.4	42.47
I	A.	Foreign Object Damage	697	350.4	30.24
		Battle damage (combat damage) Bent	23 7	262.2 373.9	0.30
		Broken	6	442.3	0.26
		Buckled	5	284.4	0.22
		Collapsed Democrad newt chin mick etc	1 297	6.0 341.2	0.04 12. 89
		Damaged part, chip, nick, etc. Dented	233	3/9.1	10.11

TABLE F-III (Cont'd)

	Reason For Removal		e With Time	Percent
		Number	MTR (Hours)	of All Causes
II.	EXTERNAL CAUSES			
i i	A. Foreign Object Damage (Cont'd) Foreign object damage Holes punched Mutiliated	81 44 0	321.9 358.3	3.51 1.91 0.00
	B. Overstressed Crash damage Hard landing Hit tree Jammed Overstressed Overtorque RPM out of limit Sudden stoppage Warped	256 2 6 1 31 2 162 49	319.1 431.5 410.5 620.0 378.0 248.0 132.5 328.6 310.1 493.0	11.11 0.09 0.26 0.04 0.04 1.34 0.09 7.03 2.13 0.09
	C. <u>Heat Demage</u> Blistered Heat Damage	- 4	494.0 765.0 403.7	0.17 0.04 0.13
	D. Maintenance and Shipping Damage Bad patch, rivet, mod, tab, etc. Damaged in shipment Improper handling	22 18 0 4	378.5 383.6 355.5	0.95 0.78 0.00 0.17
	E. Other	0	<u></u>	0.00
111.	NO FAILURE CAUSES	_33	509.4	1.43
	A. <u>Time Change</u> Allowable operating time		1,100.0 1,100.0	0.04
	B. Other Inspect, evaluate, or repair Lost or missing No failure Scheduled maintenance	32 4 8 16 4	491.0 435.8 350.2 558.4 557.8	1.39 0.17 0.35 0.69 0.17
IV.	UNKNOWN CAUSES	834	<u>461.3</u>	<u>36.18</u>

TABLE F-IV. REASON FOR REMOVAL/MTR ANALYSIS OF C/G M/R BLADES REPAIRED OR SCRAPPED AT BHC

Reason	For Removal	Record Part	s With Time	Percent Of All
		Number	MTR (Hours)	Сицвен
ALL CAUSES		606	309.4	100.0
I. PART CAUSES		124	335.0	20.5
	e Vibration pecified tolerance lance	74 	323.4 715.5 328.2	$\frac{12.2}{0.3}$
Erratic Excessiv Mismatch	e vibration ed	2 24 1	345.0 277.9 374.0	0.3 4.0 0.2
B. Deterior Cracked Deterior	eted	25 18 2	298.2 376.7 70.0	4.1 3.0 0.3
Loose ri Loose tr		4	276.0 64.3	0.2 0.7
C. Bonding Bond sep Delamina Loose	eration	18 13 2 3	371.8 410.2 20.5 439.3	3.0 2.1 0.3 0.5
	e Wear failure essively	-4 1 1 2	520.3 436.0 504.0 570.5	0.7 0.2 0.2 0.3
E. Corrosio	n corrosion	_3	461.0 461.0	0.5
P. Other				0.0
II. EXTERNAL CAU		<u>305</u>	273.8	50.3 37.8
Battle d Bent	Object Damage amage (combat damage)	229 76 3	281.4 272.0 319.3	12.5 0.5
Dented	part, chip, nick, etc.	77 30	395.0 307.4 262.6	0.2 12.7 5.0 3.5
Foreign Holes pu Mutilate		21 20 1	277.0 250.4 36.0	3.3 0.2
B. Overstre Broken w		71	261.4 599.0	11.7

TABLE F-IV (Cont'd)

Reason For Removal		With Time	Percent Of All
	Number	MTR (Hours)	Causes
B. Overstressed (cont'd) Crash damage Hard landing Hit tree Overstressed RPM out of limit Sudden stoppage C. Heat Damage D. Maintenance and Shipping Damage Damaged in shipment Improper handling E. Other III. NO FAILURE CAUSES A. Time Change Allowable operating time B. Other No Tailure Scheduled maintenance IV. UNKNOWN CAUSES	2 5 8 33 19 0 5 0 29 16 16 13 12 1	238.0 188.2 301.0 324.3 245.8 259.9 -106.2 	0.3 0.8 0.5 1.3 5.4 3.1 0.0 0.8 0.0 4.8 2.6 2.6 2.1 2.0 0.2 24.4

TABLE F-V. REASON FOR REMOVAL MTR ANALYSIS OF D H MAIN ROTOR BLADES REPAIRED AT BHC

			Record	w With	
1	Reason For Removal		Part	Time	Percent of All
			Number	(Hours)	Chuses
ALL CAU	SES		934	310.0	100.0
1.	PAR	r causes	<u>161</u>	308.8	17.2
	A.	Excessive Vibration Beyond specified tolerance	47 1	277.1 516.0	5.0 7.1
		Cannot balance Excessive vibration	26 18	315.8 203	3.0
	В.	Deterioration	33	274.	3.5
		Cracked Deteriorated		266.3 83.7	2.9 0.3
İ		Loose rivets	2	556.5	0.2
	c.	Noisy Bonding Failure	1 52	516.0 318.1	0.1 5.6
	٠.	fond separation Delaminated	41	288.4 511.4	4.4 0.7
		Loose	2	203.5	0.2
		Poor bonding	2	366.0	0.2 2.7
	D.	Excessive Wear Erosion	25 19	387.0 377.4	2.0
		Internal Failure Pirted	2 1	456.5 704.0	0.2 0.1
j	_	Worn excessively	3	296.0	0.3
	E.	<u>Corrosion</u> Deposits	$\frac{3}{2}$	395.7 479.0	$\frac{0.3}{0.2}$
	_	Rust or corrosion	1	229.0	0.1
	F.	Other Manufacturing defect	-	213.0 213.0	$\frac{0.1}{0.1}$
11.	EXI	ERNAL CAUSES	424	265.6	45.4
	A.	Foreign Object Damage Battle damage (combat damage)	<u>282</u>	272.3 121.5	$\frac{30.2}{0.2}$
		Bent	4 2	553.8 27.0	0.4
		Broken Buckled	1	6.C	0.1
		Damaged part, chip, nick, etc. Dented	1 34 1.00	277.5 288.9	14.3 10.7
		Foreign object damage	28 11	189.7 260.9	3.0 1.2
		notes penones			

TABLE F-V (Cont'd)

Reason F	or Removal		s With Time	Percent of All
		Number	MTR (Hours)	Cunken
B. Overstre Crash da Hard lan Overstre Overtorq RPM out Sudden s C. Heat Dam Blistere Heat dam D. Maintena Bad patc Improper E. Other III. NO FAILURE C A. Time Cha B. Other	mage dding sued pue of limit stoppage mage dage dage hage hace and Shipping Damage h, rivet, tab, etc. handling CAUSES mage evaluate, or repair missing	131 19 18 18 18 2 1 1 9 7 2 0 9 0 9 3 6 340	246.6 10.0 392.8 245.3 217.0 252.0 204.0 518.0 765.0 277.5 269.1 307.0 421.4 469.7 397.3 363.0	14.0 0.1 0.4 2.0 0.1 9.4 1.9 0.2 0.1 1.0 0.7 0.2 0.0 1.0 0.3 0.6 36.4

TABLE F-VI. REASON FOR REMOVAL/MIR ANALYSIS OF C/G MAIN ROTOR BLADES REPAIRED AT BHC

	Reason For Removal	Record Part	s With Time	Percent of All
		Number	MTR (Hours)	Causes
ALL GAUSE	S =	<u> 297</u>	241.4	100.0
I. P	ART CAUSES	74	241.7	24.9
^		50	240.6	$\frac{16.8}{0.3}$
	Beyond specified tolerance Can't balance	28	515.0 213.9	9.4
	Erratic Excessive vibration	1 19	223.0 259.5	0.3 6.4
	Mismatched	1	374.0	0.3
В		14	195.9	4.7
	Cracked Deteriorated	2	295.7 70.0	2.4 0.7
•	Loose rivets	1 4	276.0	0.3 1.3
	Loose trimtabs .	, ,	64.3	2.4
	Bonding Failure Bond separation	-6	209.8 241.8	2.0
	Delaminated	1	18.0	0.3
D.	. Excessive Wear Internal failure	-3	548.3 504.0	$\frac{1.0}{0.3}$
	Worn excessively	Ž	570.5	0.7
€.	. Corrosion	0		0.0
F.	• Other	_0	<u></u> -	0.0
11. <u>E</u>	XTERNAL CAUSES	123	235.6	41.4
Α.	· Foreign Object Damage	<u>68</u>	251.5 101.1	$\frac{22.9}{3.0}$
	Battle damage (combat damage) Cut	1	395.0	0.3
	Damaged part, chip, nick, etc. Dented	30 13	301.2 208.5	10.1
	Foreign object damage	10	302.6	3.4
	Holes punched	5	205.0	1.7
В.	. Overstressed Broken weights	<u>-51</u>	230.5 599.0	$\frac{17.2}{0.3}$
	Crash damage	į	344.0	0.3
	Hard landing Hit tree	1	6.0 230.0	0.3 0.3
	Overstressed	5	342.5	1.7
	RPM out of limit Sudden stoppage	30 12	238.5 142.5	10.1 4.0

TABLE F-VI (Cont'd)

Reason For Removal	Record	s With Time	Percent or All
	Number	(Hours)	Causes
G. Heat Damage D. Mathrenance and Shipping Damage Damaged in shipment Improper bandling E. Other 111. NO FALLIRE CAUSES A. Time Change B. Other IV. UNKNOWN CAUSES	0 10 10 10 10 90	29.0 29.0 306.6 306.6 306.6 242.0	0.0 1.3 0.0 1.3 0.0 3.4 7.0 3.4 3.4 30.3

TABLE F-VII. REASON FOR REMOVAL MIR ANALYSIS OF D. H MAIN ROTOR BLADES SCRAPPED AT BIC AND RRAD

		Reason For Removal		n With Time	Parce.
			Number	Mik (Hours)	di Ali
ALI. CAU	SES		1 . 886	(14.6) . 1	100.0
1.	PAR	T CAUSES	30 1	526	11.17
	Α.	Excessive Vibration Beyond specified tolerance Cannot balance Eventic	- 58 - 4 - 36 - 1	302.6 377.5 357.4 35.0	1.05
1	а.	Excessive vibration Deterioration Cracked Deteriorated Noisy	1.7 -69 -56 1.2	533.3 535.9 555.3 181.0	0.99 3.46 7.97 0.64 0.95
	c.	Bonding Failure Bond separation Delaminated Loosa	103 76 19 8	527.4 519.4 443.3 613.4	5.46 4.03 1.01 02
	D.	Excessive Wear Erosion Internal Failure Pitted Worn excessively	-53 -41 -5 -3 -4	608.6 600.9 640.6 485.6 740.5	2.81 7.17 9.17 9.16 9.21
	€.	Corrosion Deposits Leaking Rust or corrosion	16 1 1 14	767.7 119.0 530.0 631.0	0.85 7.65 0.05 0.7-
	F.	Other Manufacturing defect	-4	269.2 269.2	0.21
11.		PERNAL CAUSES	900	411.6	47.72
	۸.	Foreign Object Damage Battle damage (combat damage) Bent Broken Buckled Gollapsed Damaged part, chip, nick, etc. Dented Foreign object damage Holes punched	626 216 3 4 4 1 165 133 53 47	417.6 433.5 134.0 650.0 354.0 6.0 394.4 446.9 391.7 385.3	33.19 11.45 9.16 0.21 0.05 8.75 7.05 2.81

TABLE F-VII (Cont'd)

	Reason For Removal		s With Time	Percent
		Number	MTR (Hours)	of All Causes
111.	B. Overstressed Crash damage Hard landing Hit tree Jammed Overstressed Overtorque RPM out of limit Sudden stoppage Warped C. Heat Damage Heat damage D. Maintenance and Shipping Damage Bad patch, rivet, tab, etc. Improper handling E. Other NO FAILURE CAUSES A. Time Change Allowable operating time B. Other Inspect, evaluate, or repair Lost or missing	23 1 2	394.9 398.3 446.0 620.0 378.0 252.3 48.0 419.6 371.7 493.0 470.0 470.0 448.4 456.5 404.0 917.3 2,064.6 2,064.6 518.2 334.0 209.0	13.73 7.16 0.11 0.05 0.05 0.64 0.05 3.92 1.64 0.11 0.11 0.11 0.69 0.58 0.11 0.00 1.64 0.42 0.42 0.42 0.42 0.42
IV.	No failure Scheduled maintenance UNKNOWN CAUSES	16 4 <u>652</u>	558.4 557.8 552.1	0.85 0.21 <u>34.57</u>

TABLE F-VIII. REASON FOR REMOVAL/MTR ANALYSIS OF C/G MAIN ROTOR BLADES SCRAPPED AT BHC AND RRAD

CAUSES **Cessive Vibration Eyond specified tolerance an't balance rratic **Cessive vibration	628 61 24 1 17	MTR (Hours) 388.7 480.7 495.9 916.0	0f All Causes 100.0 9.7 3.8
excessive Vibration Eyond specified tolerance an't balance rratic	61 24 1	480.7 495.9	9.7
excessive Vibration Eyond specified tolerance an't balance rratic	24 1 17	495.9	
eyond specified tolerance an't balance cratic	17		3.0
	5	516.5 467.0 347.8	0.2 2.7 0.2 0.8
eterioration racked	14	446.4 446.4	2.2
onding Failure ond separation elaminated oose	14 10 1 3	423.0 458.1 23.0 439.3	2.2 1.6 0.2 0.5
kcessive Wear rosion	$\frac{3}{3}$	746.0 746.0	0.5 0.5
orrosion ust or corrosion	<u>6</u>	502.0 502.0	$\frac{1.0}{1.0}$
ther			0.0
NAL CAUSES	389	302.7	61.9
oreign Object Damage attle damage (combat damage) ent amaged part, chip, nick, etc. ented oreign object damage oles punched utilated	227 3 47 20 16 42	301.7 319.3 311.3 311.4 236.0 302.0 36.0	56.7 36.1 0.5 7.5 3.2 2.5 6.7 0.2
verstressed rash domage ard landing it tree verstressed PM out of limit udden stoppage	32 12 4 2 3 3 8	329.2 258.7 233.8 336.5 294.0 319.3 497.6	5.1 1.9 0.6 0.3 0.5 0.5
N OF BERNOOU VICE TO VE	rosion AL CAUSES reign Object Demage tile damage (combat damage) nt naged part, chip, nick, etc. nted reign object damage les punched tilated erstressed ash damage rd landing t tree erstressed M out of limit	rosion at or corrosion her AL CAUSES reign Object Demage ttle damage (combat damage) nt maged part, chip, nick, etc. nted reign object damage les punched tilated erstressed ash damage rd landing t tree erstressed M out of limit dden stoppage 6 389 356 227 37 47 10 40 42 42 42 42 43 44 44 45 46 47 48 49 40 40 40 41 41 41 42 43 44 44 45 46 47 48 48 49 40 40 40 40 40 40 40 40 40	10 10 10 10 10 10 10 10

TABLE F-VIII (Cont'd)

	Reason For Removal		s With Time	Percent Of All
		Number	MTR (Hours)	Свинен
	EXTERNAL CAUSES D. Maintenance and Shipping Damage Improper handling E. Other NO FAILURE CAUSES A. Time Change Allowable operating time B. Other No failure	1 0 -4/ -41 -6 -5	415.0 415.0 919.0 973.0 973.0 550.2 604.8	-0.2 -0.0 -2.5 -6.5 -1.0 -2.8
!V.	Scheduled maintenance UNKNOWN CAUSES	131	277.0 411.2	20.9

TABLE F IX. REASON FOR REMOVAL/MIR ANALYSIS OF D H MAIN ROTOR BLADES SCRAPPED AT BHO

Blades From Aircraft Model(s): UH-LD/H Part No. 204 01: -250 -- 105

				Message and the same	
		Reason For Removal		s With Time	Percent
			Number	MTR (Hours)	Caunes
ALL CAL	SES		1,371	476.0	100.00
τ.	PAR	T CAUSES	298	518.8	21.,74
	A.	Excessive Vibration Beyond specified tolerance	<u> 58</u>	$\frac{391.6}{472.5}$	$-\frac{4.23}{0.29}$
		Cannot balance	3 6	357.4	2.63
		Erratic Excessive vibration	1.7	95.0 462.4	1.24
	R.	leterioration Cracked	- <u>69</u>	533.3 534.9	5.03 4.08
İ		Deteriorated	1.2	555.3	0.88
	c.	Noisy Bonding Pailure	101	181.0 522.6	0.07 7.37
	٥.	Bond separation	101 74	733.2	5.40
ŀ		Delaminated Loose	19 8	443.3 613.4	1.39 0.58
	D.	Excessive Wear Erosion	<u>53</u> 41	608.6 600.8	3.87 2.99
ł		Internal failure	5	640.6	0.36
		Pitted Worn excessively	3 4	485.6 740.5	0.22 0.29
	E.	Corrosion	13	689.5	0.95
		Deposits Leaking	1	119.0 530.0	0.07
		Rust or corrosion	11	755.9	0.80
	P.	Other Hanufacturing defect	-4	269.2 269.2	0.29 0.29
II.	EXT	ERNAL CAUSES	<u>555</u>	402.9	40.48
	A.	Foreign Object Damage Bittle damage (combat damage)	$\frac{415}{21}$	403.5 275.6	30.27 1.53
		Bent	3	134.0	0.22
		Broken Buckled	4	650.0 354.0	0.29 0.29
ì		Collapsed Damaged part, chip, nick, etc.	l 163	6.0 393.6	0.07 11.89
		Dented Foreign object damage	133 53	446.9 391.7	9.70 3.87
		Holes punched	33	390.8	2.41
		Mutilated	n		0.00

TABLE F-IX (Cont'd)

	Reason For Removal		ls With Time	Percent
		Number	MTR (Hours)	of All Causes
11.	EXTERNAL CAUSES (Cont'd) B. Overstressed	1.25	395. 0	9.12
	Crash damage Hard landing Hit tree Jammed Overstressed Overtorque RPM out of limit Sudden stoppage Warped	1 1 1 12 1 74 31	853.0 446.0 620.0 378.0 252.3 48.0 419.6 371.7 493.0	0.07 0.15 0.07 0.07 0.89 0.07 5.40 2.26 0.15
	C. <u>Heat Damage</u> Heat Damage	$-\frac{2}{2}$	470.0 470.0	$\frac{0.15}{0.15}$
	D. Maintenance and Shipping Damage Bad patch, rivet, mod, tab, etc. Damaged in shipment Improper handling	13 11 0 2	448.4 456.5 404.0	0.95 0.80 0.00 0.15
	E. Other	0	<u></u>	0.00
111.	NO FAILURE CAUSES A. Time Change Allowable operating time	$\frac{24}{-\frac{1}{1}}$	542.4 1,100.0 1,100.0	1.75 0.07 0.07
	B. Other Inspect, evaluate, or repair Lost or missing No failure Scheduled maintenance	23 1 2 16 4	518.2 334.0 209.0 558.4 557.8	1.68 0.07 0.15 1.17 0.29
IV.	UNKNOWN CAUSES	<u>494</u>	529.0	36.03

TABLE P-X. REASON FOR REMOVAL/MTR ANALYSIS OF C/G MAIN ROTOR BLADES SCRAPPED AT BHC

Blades From Aircraft Model(s): UH-1C/AH-1G Part No. 540-011-001-005

	Reason For Removal		Record Part	s With Time	Percent
	Readon 100 Removas		Number	MTR (Hours)	Of All Causes
ALL CAU	ES		309	374.9	100.0
I.	PART CAUSES		50	473.1	16.2
	A. Excessive Vibration Beyond specified to Can't balance Erratic Excessive vibration	lerance	24 1 17 1 5	495.9 916.0 516.5 467.0 347.8	7.8 0.3 5.5 0.3 1.6
	B. <u>Deterioration</u> Cracked		11	428.3 428.3	3.6 3.6
	Bonding Failure Bond separation Delamination Loose		11 7 1 3	474.8 554.5 23.0 439.3	3.6 2.3 0.3 1.0
	D. Excessive Wear Erosion		1	436.0 436.0	0.3
	E. <u>Corrosion</u> Rust or corrosion		3	461.0 461.0	$\frac{1.0}{1.0}$
	F. Other		0_		0.0
11.	EXTERNAL CAUSES		182	299.8	58.9
	A. Foreign Object Dama Battle damage (comb Bent Damaged part, chip, Dented Foreign object dama Holes punched Mutilated	at damage) nick, etc.	161 67 3 47 17 11 15 1	294.0 295.0 319.3 311.3 303.9 253.7 265.5 36.0	52.1 21.7 1.0 1.2 5.5 3.6 4.9 0.3 6.5
	B. Overstressed Crash damage Hard landing Hit tree Overstressed RPM out of limit Sudden stoppage		1 4 2 3 3 7	340.4 132.0 233.8 336.5 294.0 319.3 461.2	0.3 1.3 0.7 1.0 1.0
	C. <u>Heat Damage</u>			-	0.0

TABLE F-X (Cont'd)

	Reason For Removal		ls With Time	Percent
		Number	(Hours)	of All Causes
11.			415.0	0.3
	D. Maintenance and Shipping Damage Improper handling E. Other	+	मां डॉ.त	0.3 0.3 0.0
111.		<u>''</u> 19	897.5	6.1
	A. Time Change Allowable operating time	16 16	972.3	5.2
	B. Other No failure Scheduled maintenance	$\frac{3}{2}$	498.3 609.0 277.0	1.0 0.7 0.3
IV.	UNKNOWN CAUSES	58	354.5	18.8

TABLE F-XI. REASON FOR REMOVAL/MIR ANALYSIS OF D/H MAIN ROTOR BLADES SCRAPPED AT RRAD

Blades From Aircraft Model(s): UH-1D/H Part No. 204-011 250-005

	Reason For Removal		ls With Time	Percent
	Readon 10. Removat	Number	MIR (Hours)	Of All Causes
ALL CAU	SES	51.5	516.2	100.0
1.	PART CAUSES	5	971.6	1.0
1	A. Excessive Vibration B. Deterioration	0		0.0
	C. Bonding Failure Bond separation	<u>-</u> <u>-</u> <u>-</u> <u>-</u> <u>-</u>	769.5 769.5	0.4
	D. Excessive Wear	0	<u></u> -	0.0
ł	E. Corrosion Rust or corrosion	-3	1,106.3 1,106.3	$\frac{0.6}{0.6}$
ł	F. Other	0		0.0
11.	EXTERNAL CAUSES	345	425.8	(0.0
	A. Foreign Object Damage Battle damage (combat damage) Damaged part, chip, nick, etc. Holes punched	211 195 2 14	445.4 450.5 463.0 372.4	41.0 37.9 0.4 2.7
	B. Overstressed Crash damage	134 134	394.9 394.9	26.0 26.0
	C. Heat Damage	0		0.0
	D. Maintenance and Shipping Damage E. Other	<u> </u>		0.0
111.	NO FAILURE CAUSES A. Time Change Allowable operating time		2,202.4 2 '02.4 02.4	1.4 1.4
Ì	B. Other	0		0.0
IV.	UNKNOWN CAUSES	158	624.4	39.7

TABLE F-XII. REASON FOR REMOVAL/MTR ANALYSIS OF C/G MAIN ROTOR BLADES SCRAPPED AT RRAD

Blades From Aircraft Model(s): UH-1C/AH-1G Part No. 540-011-001-005

					-
		Reason For Removal		s With Time	Percent of All
			Number	MTR (Hours)	Causes
ALL CAU	SES		<u>319</u>	402.2	100.0
ı.	PAR	RT CAUSES	11	515.3	3.4
	A.	Excessive Vibration	_0		0.0
	В.	Deterioration Cracked	$-\frac{3}{3}$	$\frac{512.6}{512.6}$	0.9
	c.	Bonding Pailure Bond separation	$-\frac{3}{3}$	$\frac{233.3}{233.3}$	0.9
	D.	Excessive Wear Erosion	$-\frac{2}{2}$	901.0 901.0	$\frac{0.6}{0.6}$
	E.	Corrosion Rust or corrosion	$-\frac{3}{3}$	543.0 543.0	0.9
i	F.	Other	0		0.0
II.	EX1	TERNAL CAUSES	207	<u>305.3</u>	64.9
	A.	Foreign Object Damage Battle damage (combat damage) Dented Foreign object damage Holes punched	195 160 3 5 27	305.0 304.5 354.0 197.0 322.3	61.1 50.2 0.9 1.6 8.5
	В.	Overstressed Crash damage Sudden stoppage	12 11 1	310.4 270.2 752.0	3.8 3.4 0.3
	C.	Heat Damage	_0		0.0
	D.	Maintenance and Shipping Damage			0.0
	E.	Other	0	<u></u>	0.0
III.	NO	FAILURE CAUSES	26	933.6	8.8
	۸.	Time Change Allowable operating time	25 25	973.4 973.4	7.8 7.8
	B.	Other No failure	$\frac{3}{3}$	602.0 602.0	0.9
IV.	UNK	NOWN CAUSES	<u>73</u>	456.2	<u>22.9</u>

APPENDIX G

DETAILS OF REASON FOR SCRAPPAGE ANALYSIS OF BELL HELICOPTER COMPANY MAIN ROTOR BLADE SCRAP DATA

TABLE G-I. REASON FOR SCRAPPAGE OF D/H MAIN ROTOR BLADES PROCESSED BY BHC AND RRAD

Model UH-1D/H

Dwg./Part No. 204-011-250-005

		ACON TOR CORADDAGE	No. of	Blades	Scrapped
	K	EASON FOR SCRAPPAGE	RRAD	внс	Total
ALL CAL	SES		1453	1420	2873
I.	PAR	RT CAUSES	208	1042	1250
	A.	Imbalance Bushing out of alignment Can't balance Tip or edge heavy Beyond specified tolerance		13 1 1 3 8	13 1 1 3 8
	В.	Deterioration Cracked Rough	<u>2</u>	35 34 1	-37 -34 3
	C.	Bonding failure Core separation Delaminated Separated	15 10 5	81 2 1 39 38	96 1 1 49 43
	D.	Void Corrosion Corroded	191 191	287 287	478 478
	E.	Water Contamination Water in blade	<u> </u>	<u>626</u>	626 626
11.	EXT	TERNAL CAUSES	1227	343	<u>1570</u>
	۸.	Foreign Object Damage Bullet holes Creased	959 483	203 42 1	1162 525 1
		Cut	5	19	24
		Damaged Den t	7	7 17	14 17
		Foreign object damage Holes	1 462	5 81	6 543
		Scored Torn	1	5 26	5 27
	B .	Overstressed Bent	268	<u>140</u>	408
		Bowed Broken Buckled Crash damage Crushed core	254	12 3 7 8	12 3 7 254 8

TABLE G-I (Cont'd)

		No. of	Bladen	Scrapped
	REASON FOR SCRAPPAGE	RRAD	BHC	Total
II.	EXTERNAL CAUSES			
	B. Overstressed (Cont'd) Distorted Mutilated Warped	14	71 21 5	85 21 5
111.	NO FAILURE CAUSES A. Time Change Allowable operating time	$\frac{11}{11}$	<u>4</u> -4	$\frac{15}{15}$
IV.	OTHER CAUSES A. Unknown	7	31	38 38

TABLE G-II. REASON FOR SCRAPPAGE OF C/G MAIN ROTOR BLADES PROCESSED BY BHG AND RRAD

Model: UH-1C/AH-1G

Day./Part No. 540-011-001-005

			No. of	Bludes	Scrupped
	REASON FOR SO	CRAPPAGE.	RRAD	BHC	Total
ALL CAU	SES		634	341	97'
I.	PART CAUSES		18	102	120
	A. Imbalance Weights lo	nos e		$-\frac{3}{3}$	$\frac{3}{3}$
	B. <u>Deterioral</u> Cracked Worn	tion		$\frac{22}{16}$	$\frac{22}{16}$
	C. Bonding Fa Separated Void	ailure	-6	- 6 - 1 5	-12 7 5
	D. Corrosion Corroded		$\frac{12}{12}$	<u>50</u> 50	$\frac{-62}{62}$
	E. Water Cont Water In	tamination blade		$\frac{21}{21}$	$\frac{21}{21}$
II.	EXTERNAL CAUSI	<u>es</u>	560	194	754
	A. Foreign Ol Bullet ho Greased	bject Damage Les	536 353	157 53 2	693 406 2
	Cut Damaged Dent		2 1	18 3 13	20 4 1.3
		bject damage	180	1 55 1 11	235 1 11
	B. Overstress Bent	s ed		37 4 3	<u>-61</u>
	Broken Crash dama	age	22	3	3 22
	Crushed control Distorted Mutilated	or?	2	1 14 15	1 16 15
III.	NO PAILURE CAL	USES	53	20	73
	A. Time Chang	ge operating time	<u> 53</u> 53	20 20	- 73

TABLE G-II (Cont'd)

	Mo. of	Blades	Scrapped
REASON FOR SCRAPPAGE	RRAD	BHC	Total
ALL CAUSES (Cont'd)			
IV. OTHER CAUSES A. Unknown	3	<u>25</u> _25	28

TABLE G-III. REASON FOR REMOVAL VS. REASON FOR SCRAPPAGE OF D/H MAIN ROTOR BLADES PROCESSED BY BHC

Blades from Aircraft Model(s): UM-1D/H				ļ					P. 4	Part %	20-	C.L250	
REASON FOR REPOVAL	131			1/1/2/		1 2 0	13/3/	1 / 2 /	1.18				1 May
ALL CAUSES	1420	1042	21	Z#	9:	797	929	E.	203	9	,,	- TE	
I. PART CAUSES	291	250	7	7	1.8	32	:3:	38	2.2	- -	(ر ،	6	
A. Excessive Vibration beyond specified tolerance	25	2	ત્ના.	7	.ال	와'	뭐.	' '†'	٠٠٠	"	نان ا	مان ا	
Can't balance Erratic Erratic	35	80 ž	~ I ~		~ 1	an ı,	ឧ ' :	en . 1 c		n 1 .	00	000	
B. Deterioration	3	3	۱، ۰	l.	· എ	· #	: #	· :4	' "	• •) (a)	, .1	
Deteriorated	127	327		· · ·	7 1 1	76.	, a	inc	4 - 4 - 1	/1 - 4 - 4	. i ()	10-	
C. Bonding Failure Bond separation Delaminated	100 73 19	92 68 16	1111	4	60 - 1 -	# 200	ျခုပ္	1/11/20	7	1 "	4 7	, 4	
D. Excessive Wear	° 28	3	' '	· -	۱۰ ۲	` ##	' ដូ	· :1	<u>' ' '</u>	· ဤ	ə ()	. 1	
Internal failure Pitted	,,,,,,	3 4 11 1		• • •	1 1 -	<u> </u>	ŋ # ci -	,,,00	1 1) () () ()	,,,,,	
Corrosion Deposits	71	' 干'	<u>'</u> ' '	1	٠ .١.	٠ ५٠	· m·	၁ ၁၁	٠ ॥٠	. 4.	, ભુ	, .1	
Leaking Rust or Corrosion	-2	76	• •	• •		ra Fi		၁၀	, ,		00	.,,•	
F.: Other Manufacturing defect	44	4 4	11.	111	11.	11.	7	00	11'	1	ajo		
II. ENTERNAL CAUSES A. Forsign Object Demage Lattle damage (combat damage) Bent Broken Buckled	S8 244 262 2 4 4	381 277 0 1 1 0	ના એ : ' ' '	ងានាប្រ	왕 지 · · ·	8 2	워크(· · ^ ·	8 34 a 3			a de con	· • •···	

TABLE G-III (Cont'd)

] ' ' ' ' ' ' ' '
	Signatura (April 2) in the management of the first of the second of the
	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
1 / 1 / 0	13% or thronors, in marrial dechi
1 / /3/4/	1950 m 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
1/1/1/	1000-11 de la la la la la la la la la la la la la
	- 5 1 8 1 5 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6
	45888 3 14445 5 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Blades from Aircraft Model(s): UH-15 H REASON FOR REMOVAL	A. Foreign Object Danage (Cont'd) Collapsed Danaged part, chip, nick, etc. Danaged part, chip, nick, etc. Danaged part, chip, nick, etc. Foreign object danage Roteign danage Roteign danage Roteign object danage Roteign object danage Roteign object Sudden stoppage Warped C. Heat Danage Roteign stoppage Warped Roteign of limit Sudden stoppage Warped C. Heat Danage Roteign of limit Sudden stoppage Warped Roteign of limit Sudden stoppage Warped C. Heat Danage Roteign of limit Sudden stoppage Warped C. Heat Danage Roteign of limit Sudden stoppage Warped Roteign object R

TABLE G-III (Cont'd)

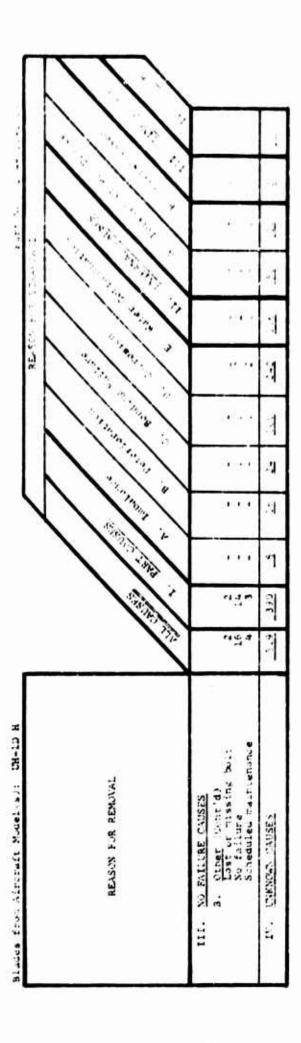


TABLE G-IV. REASON FOR REMOVAL VS. REASON FOR SCRAPPAGE OF C/G MAIN ROTOR BLADES PROCESSED BY BHC

Blades from Aircraft Model(s): UM-1C/AH-1G				Į						ij	No.: 5-6	35	
REASON FOR REMOVAL	13			1/4/4/	10.11.10.1	1 37 4 4 3 1	135 13	1 1 1 1		13/2/		13/1	18/18/
ALL CAUSES	ᆒ	201	-JI	뭬	911	SII	ᅰ	:6:	91	5	<u>26</u>	23	
I. PART CAUSES	53	29	۲۱	~	ы	2	•	3	di	•	.,		
A. Excessive Vibration Seyond specified tolerance	2	910	111	1'1'	ला	의'	ग	~	17	17	1 "†	14	
Can't balance Erratic	17	`# 	• •	٦ ۱	-4 4	***	7) vi ¢	ra (. ~ .	1-1-5	100	
Excessive vibration		.7	•	•	•	• • •	14) (j	•			, ,	
B. Deterioration Cracked	::‡:	**	11	~ ~	17.	• •	.1.	۰۴۰	**	or	1	**	
C. Bonding Failure Bond separation Delaminated Loose	10 11 1	ماس⊶-		11''	4	Merce	11	11100	· ~			ေချခ	
D. Excessive Wear	0	• 0	, ,	• •		•		n (4	r (() ()	c) (
	1 34	177	1 41	177	1 11.	1 1.	111	11	1.1.	11-4.	4.4.	기이 .	
P. Other	9	이	-1	-1	÷	<u> </u>		Ü	1	1	ી	의	
II. EXTERNAL CAUSES A. Foreign Object Demage Battle demage (combet demage)	3 22	គ ក	7 -	의학	44	នានា	ा अन	別語	21 :12	ងនា'	બ બ	ા ન	
Danaged part. chip. nick. etc. Danaged	m eg ?	- <u>1</u> 2 4		4		1.3	• •	~ SE	'n	C4 . 4 ·	a o	·=•	
Foreign object damage Moles punched Mutilated	322-	0 t. W		1 77 1		100	1 1	11° 31°	7010		0 200	1.594	
B. Overstressed Crash damage Hard landing	2113	70%	417	7917	4	٠٠٠			. 1	i vijes.) up - c	400	
Mit tree Overstressed APM out of limit Sudden stoppage	nn-1	0 11 11 10	1411				1 1 1 1 4	9000			, () 1 () 5	, ili,	
									•	•		,	

TABLE G-IV (Cont'd)

Blades from Aircraft Model(s): UH-1C/AH-1G				Į	١	١				Part No		546-51603	:
REASON FOR REMOVAL	13				1 1 1 1 1	18.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	- 1 647 1 Sta	2 / / 1. /	San San San San San San San San San San	13/10/	10010	1 1/3/1	1/1/18
II. EXTERNAL CAUSES C. Mest Damage D. Maintenance and Shipping Improper handling E. Other	이삭이	ીજ ગ	44.4	기반기	44.4	11:1	ग कुल	이수이	14.4	44.4	. ગુભુગ	ા અગ્	
III. NO FAILURE CAUSES A. Time Change Allowable operating time B. Other No failure Scheduled maintenence	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14-40-	44.4.	444	11.4.	m 11. mara	44.4.	mm, 400	44.4.	17.1.	계:학: 역으로	J J 100	
IV. UNKNOWN CAUSES	7.9	30	1	7	1	21	커	ङ	#1	4	7	31	

APPENDIX H

DETAILS OF THE PROBABILITY OF SCRAPPAGE AND REPAIR ANALYSES OF MAIN ROTOR BLADES REMOVED IN VIETNAM

TABLE H-I. REASONS FOR REMOVAL VERSUS NUMBER OF DZH MAIN ROTOR BLADES REMOVED, SCRAPPED, SHIPPED AND REPAIRED

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TABLE H-I (Cont'd)

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	Total	Removana	Organiza	it ion	Red	Red b. er	*	* : A.F *	4		* 1	٠		
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II. EXTERNAL CAUSES (Cont'd)	ç	ć	•				٠,							
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TABLE H-II. REASONS FOR REMOVAL VERSUS NUMBER OF C/G MAIN ROTOR BLADES REMOVED, SCRAPPED, SHIPPED AND REPAIRED

Part No.: 5-6-6...-001-5

Blades From Aircraft Model(s): UH-1C/AH-1G

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	Reason for amoval	COMBINED CAUSES*		II. EXTERNAL CAUSES A. Foreign Object Damage Battla damage Bent Broken Chipped Cut Dented Foreign object damage Nicked Punctured

* Part and External Causes Only

TABLE H-II (Cont'd)

Blades From Aircraft Model(s): UH-1C/AH-1G	H-1G					i						Part No	.: 540-	Part No.: 546-011-301-5
		Removing Organization	Organiz	ation	Red	Red River	2	epair F	Repair Facility	ĺ	E-W	781 ~2		•*
Reason for Removal	Removed	Repair.	Scrap. Ship.	Ship.	Held S	Held Scrap. Pud.	F.	Repair.	Scrap.		Held Fud.	Repair. Scrap.	Scrap.	Repaired
II. EXTERNAL CAUSES (Cont'd)														•
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failures are reported in terms of cause, fr	
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